

### DESCRIPTION

The HF300 is an intelligent, high-frequency, flyback, ideal clamping controller that is used to replace the passive resistor-capacitor-diode (RCD) snubber in a flyback circuit to clamp the drain-source voltage spike caused by the leakage inductance ( $L_{LKG}$ ) after the primary main switch turns off. The HF300 is compatible with many flyback operating modes, such as continuous conduction mode (CCM), discontinuous conduction mode (DCM), quasi-resonant (QR) operation, and zero-voltage switching (ZVS). The HF300 can support up to 300kHz flyback applications, and can also improve the efficiency of a flyback circuit.

The HF300 is the ideal substitute for a traditional passive RCD snubber. Replacing this traditional snubber does not bring increase complexity and or system cost.

Full protection features and flexible parameter settings guarantee safe operation of the flyback circuit.

The HF300 is available in a space-saving TSOT23-6 package.

### FEATURES

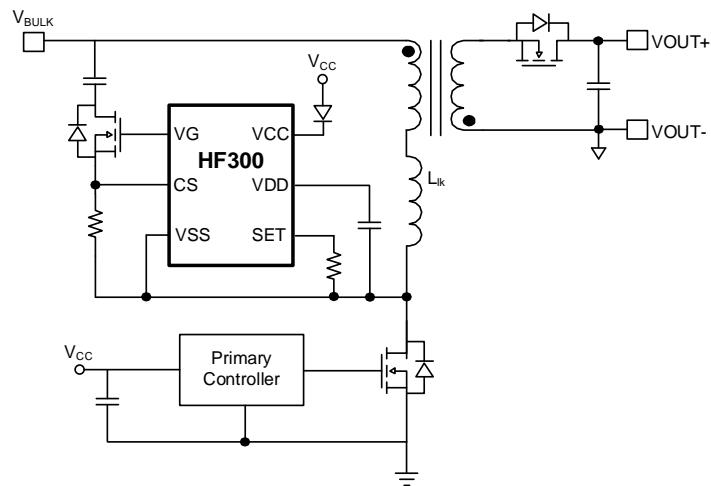
- Active-Clamp Drain-Source Voltage Spike
- Supports Continuous Conduction Mode (CCM), Discontinuous Conduction Mode (DCM), Quasi-Resonant (QR) Operation, and Zero-Voltage Switching (ZVS)
- Supports Up to 300kHz Switching Frequency ( $f_{SW}$ )
- Easy to Use
- Extremely Low  $<5\text{mW}$  Standby Power Consumption
- Ultra-Wide VCC Range to Support USB PD Applications
- Intelligent Recycling Leakage Energy and Increased Flyback Converter Efficiency
- Under-Voltage Lockout (UVLO), Over-Current Protection (OCP), and Shoot-Through Prevention
- Available in a TSOT23-6 Package

### APPLICATIONS

- USB Power Delivery (PD)/Quick Charge (QC) Chargers and Adapters
- Adapters
- High Power Density Flyback Power Supplies

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### TYPICAL APPLICATION



**ORDERING INFORMATION**

Part Number*	Package	Top Marking	MSL Rating
HF300GJ	TSOT23-6	See Below	1

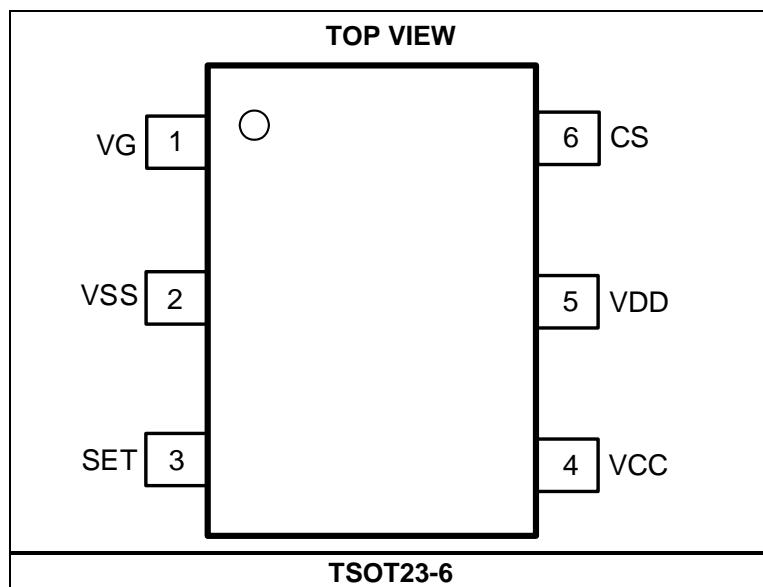
\* For Tape & Reel, add suffix -Z (e.g. HF300GJ-Z).

**TOP MARKING**

| BXEY

BXE: Product code of HF300GJ

Y: Year code

**PACKAGE REFERENCE**

**PIN FUNCTIONS**

Pin #	Name	Description
1	VG	<b>Gate driver output.</b>
2	VSS	<b>IC ground.</b>
3	SET	<b>Configuration pin.</b> Connect the SET pin to a resistor.
4	VCC	<b>IC power supply.</b>
5	VDD	<b>Gate driver power regulator output.</b>
6	CS	<b>Current sensing.</b> The CS pin turns VG on and off.

**ABSOLUTE MAXIMUM RATINGS <sup>(1)</sup>**

VCC to VSS .....	-0.3V to +180V
VDD, VG to VSS .....	-0.3V to +12V
CS to VSS .....	-3V to +6.5V
SET to VSS .....	-0.3V to +6.5V
Continuous power dissipation ( $T_A = 25^\circ\text{C}$ ) <sup>(2)</sup> .....	0.56W
Junction temperature ( $T_J$ ) .....	150°C
Lead temperature .....	260°C
Storage temperature .....	-55°C to +150°C

**ESD Ratings**

Human body model (HBM) .....	2000V
Charged-device model (CDM) .....	2000V

**Recommended Operating Conditions <sup>(3)</sup>**

Supply voltage ( $V_{CC}$ ) .....	7.5V to 90V
CS to VSS .....	-1 to +0.5V
Maximum junction temperature ( $T_J$ ) .....	125°C

**Thermal Resistance <sup>(4)</sup>  $\theta_{JA}$   $\theta_{JC}$** 

TSOT23-6 .....	220 .... 110.. °C/W
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**Notes:**

- 1) Exceeding these ratings may damage the device.
- 2) The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_J$  (MAX), the junction-to-ambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_A$ . The maximum allowable continuous power dissipation at any ambient temperature is calculated by  $P_D$  (MAX) =  $(T_J$  (MAX) -  $T_A$ ) /  $\theta_{JA}$ . Exceeding the maximum allowable power dissipation can produce an excessive die temperature, which may cause the regulator to go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- 3) The device is not guaranteed to function outside of its operating conditions.
- 4) Measured on a JESD51-7, 4-layer PCB.

## ELECTRICAL CHARACTERISTICS

 $T_J = -40^\circ\text{C}$  to  $+125^\circ\text{C}$ , typical values are tested at  $T_J = 25^\circ\text{C}$ , unless otherwise noted.

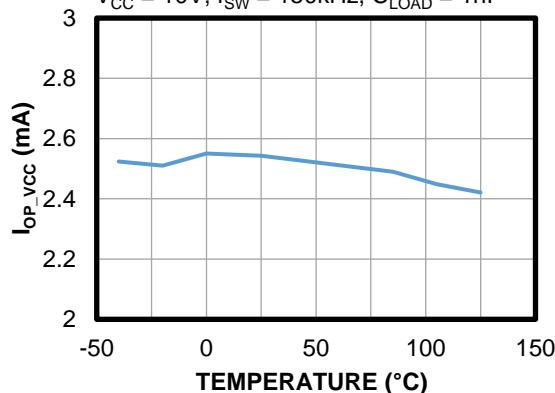
Parameter	Symbol	Condition	Min	Typ	Max	Units
<b>Supply Voltage Management (VCC and VDD Pins)</b>						
VCC maximum charging current		$V_{DD} = V_{DD\_START}$ , $V_{CC} = 10\text{V}$	20			mA
VDD start-up threshold	$V_{DD\_START}$			5.15	5.4	V
VDD voltage ( $V_{DD}$ ) under-voltage lockout (UVLO) hysteresis	$V_{DD\_HYS}$			0.5		V
VDD regulation voltage	$V_{DD\_REG}$	$V_{CC} = 10\text{V}$	7.6	8	8.6	V
VCC operating current	$I_{OP\_VCC}$	$V_{CC} = 10\text{V}$ , $f_{SW} = 150\text{kHz}$ , $C_{LOAD} = 1\text{nF}$			3	mA
VDD quiescent current	$I_{Q\_VDD}$	$V_{CC} = 0\text{V}$ , $R_{SET} = 45\text{k}\Omega$ , $V_{DD} = V_{DD\_REG}$		150	200	$\mu\text{A}$
VDD shutdown current	$I_{SD\_VDD}$	$V_{DD} = V_{DD\_UVLO} - 0.1\text{V}$ (5)			80	$\mu\text{A}$
<b>Gate Driver (VG Pin)</b>						
Driver voltage high level	$V_{G\_HIGH}$	$C_{LOAD} = 1\text{nF}$ , $V_{DD} = V_{DD\_UVLO} + 0.1\text{V}$ (5)	4.6			V
		$C_{LOAD} = 1\text{nF}$ , $V_{DD} = 8\text{V}$		8		V
Driver voltage low level	$V_{G\_LOW}$	$C_{LOAD} = 1\text{nF}$ , $V_{DD} = 8\text{V}$			0.02	V
Pull-up resistance				3		$\Omega$
Pull-down resistance				1		$\Omega$
<b>Current Sense (CS Pin)</b>						
Gate driver turn-on threshold	$V_{CS\_ON}$		-50		-10	mV
Turn-on delay	$t_{ON\_DELAY}$	$C_{LOAD} = 1\text{nF}$		75		ns
Zero-current detection (ZCD) threshold to turn-off the gate driver	$V_{CS\_ZCD}$			10		mV
ZCD turn-off delay	$t_{OFF\_DELAY}$	$C_{LOAD} = 1\text{nF}$		70		ns
Over-current protection (OCP) and shoot-through prevention threshold	$V_{CS\_OCP}$		0.7	0.8	0.9	V
OCP and shoot-through prevention turn-off delay	$t_{OCP\_DELAY}$	$C_{LOAD} = 1\text{nF}$		60		ns
Leading edge blanking (LEB)	$t_{LEB}$			230		ns
<b>Time Configuration (SET Pin)</b>						
SET pin voltage	$V_{SET}$	$R_{SET} = 124\text{k}\Omega$		1.23		V
Maximum turn-on time	$t_{ON\_MAX}$	$R_{SET} = 24.9\text{k}\Omega$	0.36	0.52	0.68	$\mu\text{s}$

**Note:**5)  $V_{DD\_UVLO} = V_{DD\_START} - V_{DD\_HYS}$ .

## TYPICAL CHARACTERISTICS

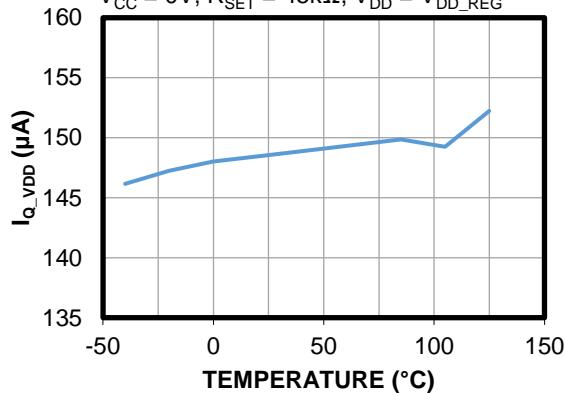
**VCC Operating Current vs. Temperature**

$V_{CC} = 10V$ ,  $f_{SW} = 150\text{kHz}$ ,  $C_{LOAD} = 1\text{nF}$

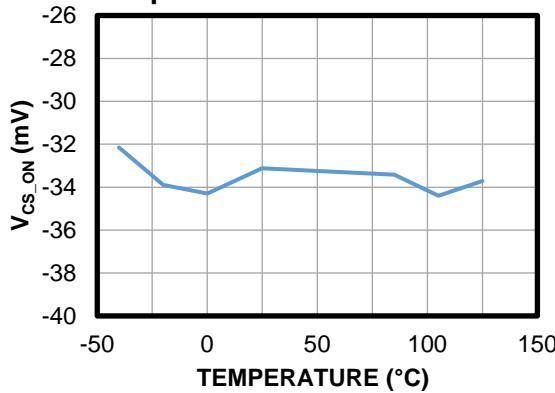


**VDD Quiescent Current vs. Temperature**

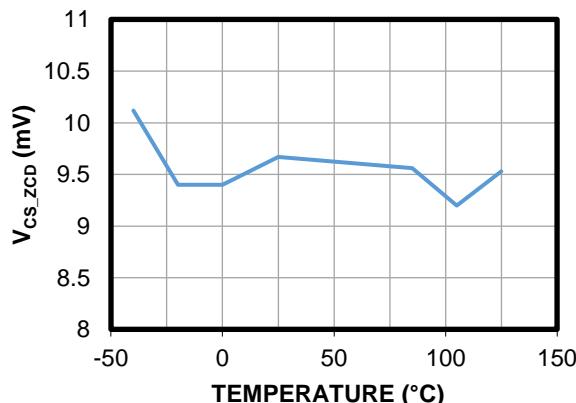
$V_{CC} = 0V$ ,  $R_{SET} = 45\text{k}\Omega$ ,  $V_{DD} = V_{DD\_REG}$



**Gate Turn-on Threshold vs. Temperature**

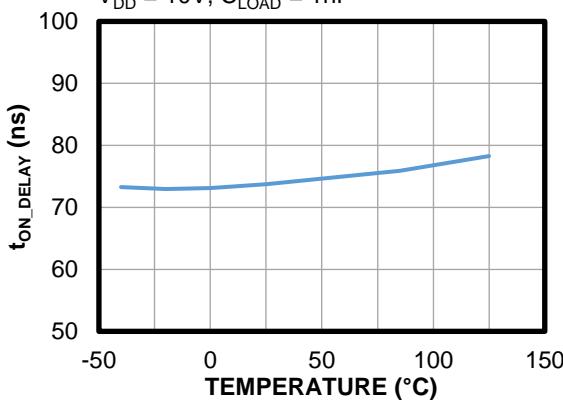


**ZCD Threshold vs. Temperature**



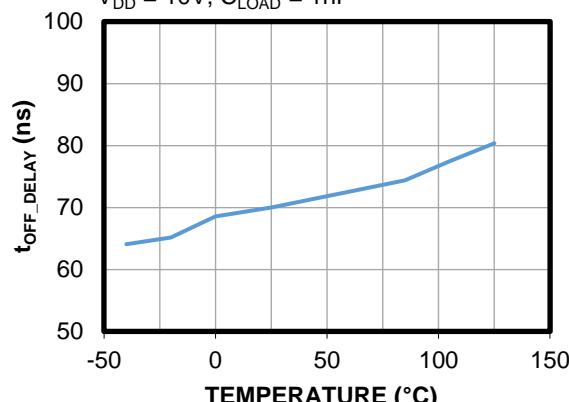
**Turn-On Delay vs. Temperature**

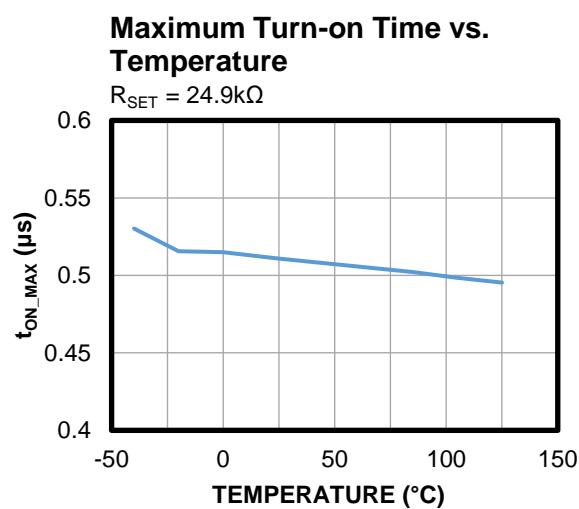
$V_{DD} = 10V$ ,  $C_{LOAD} = 1\text{nF}$



**ZCD Turn-Off Delay vs. Temperature**

$V_{DD} = 10V$ ,  $C_{LOAD} = 1\text{nF}$

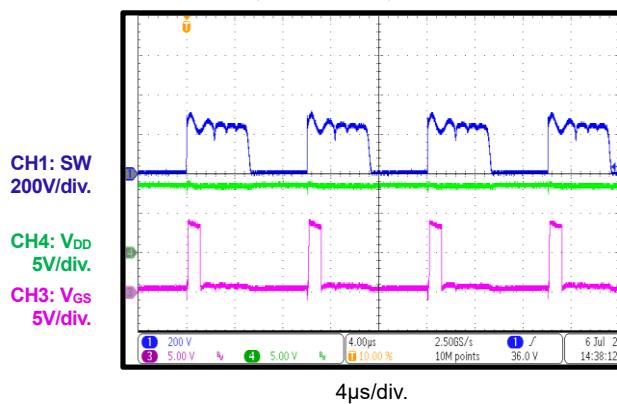


**TYPICAL CHARACTERISTICS (continued)**

## TYPICAL PERFORMANCE CHARACTERISTICS

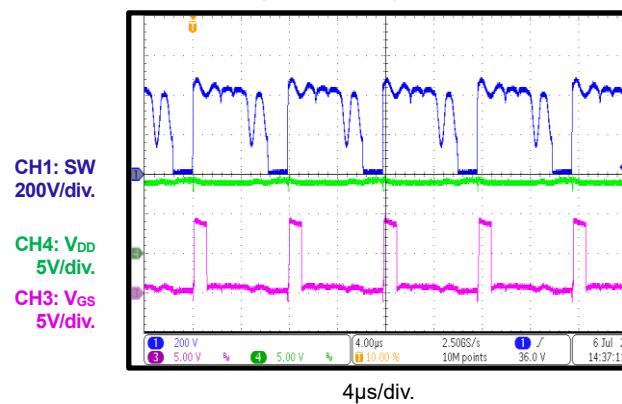
### 65W QR Flyback Application Operation

$V_{IN} = 110V_{AC}$ ,  $V_{OUT} = 20V$ ,  $I_{OUT} = 3.25A$



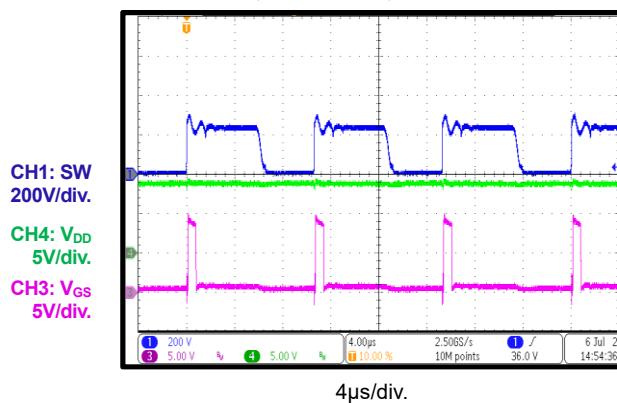
### 65W QR Flyback Application Operation

$V_{IN} = 220V_{AC}$ ,  $V_{OUT} = 20V$ ,  $I_{OUT} = 3.25A$



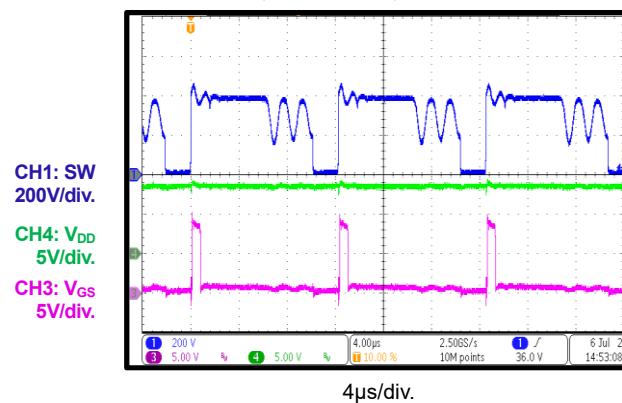
### 120W QR Flyback Application Operation

$V_{IN} = 110V_{AC}$ ,  $V_{OUT} = 20V$ ,  $I_{OUT} = 6A$



### 120W QR Flyback Application Operation

$V_{IN} = 220V_{AC}$ ,  $V_{OUT} = 20V$ ,  $I_{OUT} = 6A$



## FUNCTIONAL BLOCK DIAGRAM

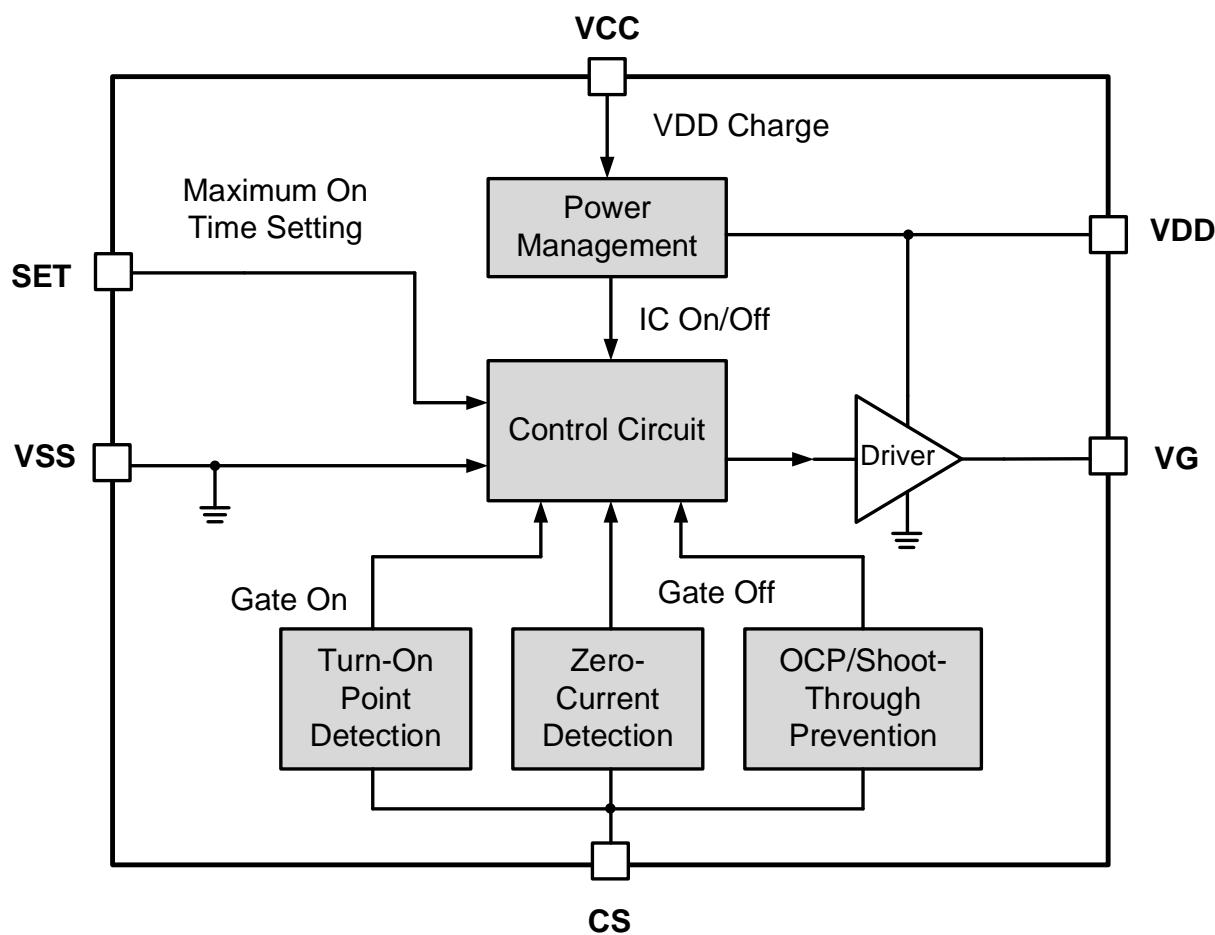


Figure 1: Functional Block Diagram

## OPERATION

The HF300 is an intelligent, high-frequency, flyback ideal clamping controller that recycles and reuses the leakage energy based on charge balance control. The HF300 supports discontinuous conduction mode (DCM), continuous conduction mode (CCM), quasi-resonant (QR) operation, and zero-voltage switching (ZVS) in flyback converters. Figure 2 shows the typical application circuit. Figure 3 and Figure 4 on page 10 show the HF300's key operating waveforms.

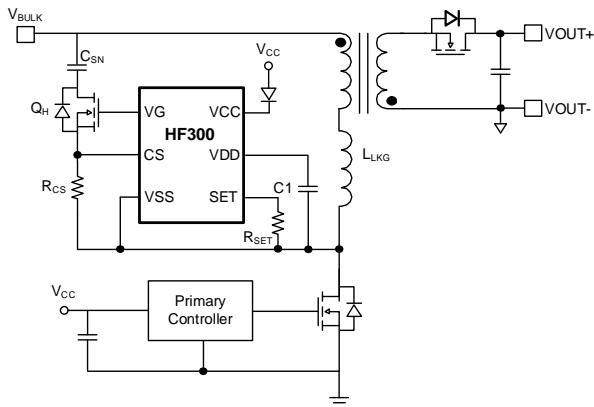


Figure 2: Typical Application Circuit

### Power Supply

VCC is the linear regulator's input, and VDD is the regulator's output. VCC charges up the capacitor at VDD through built-in high voltage (HV) current source. VDD supplies power to the HF300, which is regulated at the VDD regulation voltage ( $V_{DD\_REG}$ ).

### Start-Up and Under-Voltage Lockout (UVLO)

VCC is connected to the primary controller's VCC supply capacitor through a bootstrap (BST) circuit. When the primary controller activates, the HV current source starts to charge VDD. Once the VDD voltage ( $V_{DD}$ ) exceeds the VDD start-up threshold ( $V_{DD\_START}$ ), the HF300 exits under-voltage lockout (UVLO) and is enabled. There is a  $V_{DD}$  UVLO hysteresis ( $V_{DD\_HYS}$ ) when the HF300 enters UVLO from an enabled state. If  $V_{DD}$  drops below ( $V_{DD\_START} - V_{DD\_HYS}$ ), the HF300 enters UVLO, and the gate driver voltage ( $V_{GS}$ ) is pulled down.

### Gate Driver

The driver capability is specified in the Electrical Characteristics section on page 4.  $V_{GS}$  is clamped internally at the driver voltage high level

( $V_{G\_HIGH}$ ) to guarantee that the external MOSFET can operate safely and reduce the internal power supply's VCC operating current ( $I_{OP\_VCC}$ ) and power loss.

### Turn-On Phase

Once the HF300 is enabled, the CS pin senses the current from the leakage inductance ( $L_{LKG}$ ) after the primary main switch turns off. When the CS pin voltage ( $V_{CS}$ ) reaches the turn-on threshold ( $V_{CS\_ON}$ ), the gate driver turns on after a turn-on delay ( $t_{ON\_DELAY}$ ) (see Figure 3).

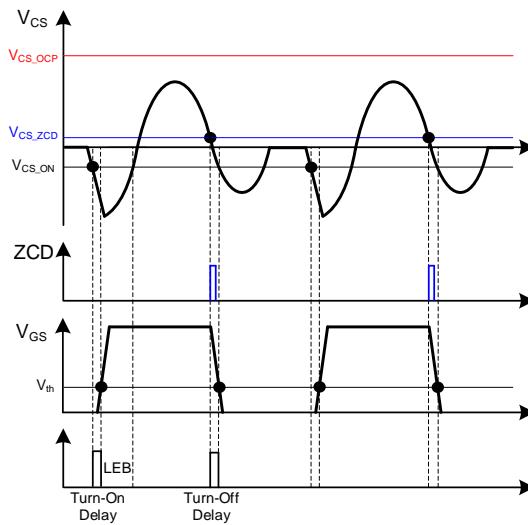


Figure 3: Key Operating Waveforms

### Leading Edge Blanking (LEB)

The control circuitry contains a blanking function. To avoid accidental, premature turn-off by the switching noise, an internal leading-edge blanking (LEB) unit is employed after the gate driver turns on (see Figure 3). During the blanking time, the turn-off comparator is disabled, and the gate driver cannot turn off.

### Conduction Phase and Turn-Off Phase

During gate driver turn-on, the leakage energy is recycled into the clamping capacitor ( $C_{SN}$ ), and then sent to the secondary-side output through a transformer when the leakage current ( $I_{LKG}$ ) has a negative resonance (i.e. the opposite direction/polarity). When the leakage is fully recycled and delivered again to the output,  $I_{LKG}$  resonates back to 0A, and the gate driver turns off (see Figure 3).

When  $V_{CS}$  reaches the zero-current detection threshold ( $V_{CS\_ZCD}$ ), the gate driver turns off after a turn-off delay ( $t_{OFF\_DELAY}$ ) (see Figure 3 on page 9).

### Cycle-by-Cycle Over-Current Protection (OCP)

The HF300's cycle-by-cycle over-current protection (OCP) limits the  $C_{SN}$  maximum discharge current. Once  $V_{CS}$  reaches the OCP/shoot-through prevention threshold ( $V_{CS\_OCP}$ ), the gate driver turns off after the OCP/shoot-through prevention turn-off delay ( $t_{OCP\_DELAY}$ ) (see Figure 4).

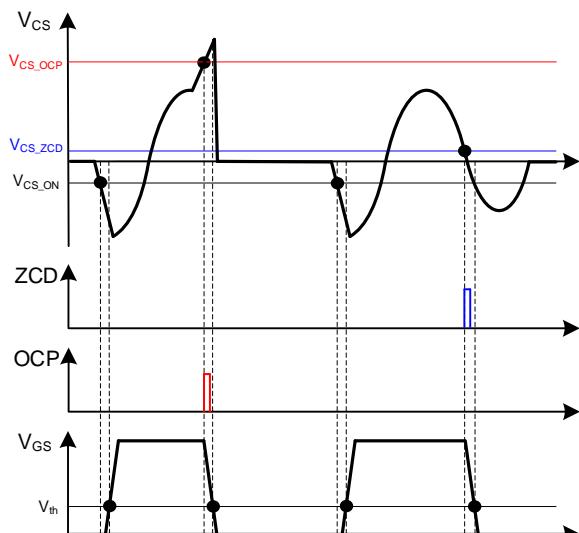


Figure 4: OCP/Shoot-Through Prevention

### Configurable Maximum Turn-On Time

To enhance system reliability and support various applications (e.g. applications with a different switching frequency [ $f_{sw}$ ] or leakage inductance), the HF300 has the flexibility to set up the maximum turn-on time ( $t_{ON\_MAX}$ ) through the SET pin's resistor ( $R_{SET}$ ).

$t_{ON\_MAX}$  ( $\mu$ s) can be configured with Equation (1):

$$t_{ON\_MAX} = (0.015 \times R_{SET} + 140) \times 10^{-3} \quad (1)$$

Once the gate driver turn-on time reaches  $t_{ON\_MAX}$ ,  $V_{GS}$  is pulled down immediately. The maximum turn-on time ensures that the HF300's gate driver can turn off safely, regardless of whether  $V_{CS}$  does not detect  $V_{CS\_ZCD}$  and  $V_{CS\_OCP}$ .

## APPLICATION INFORMATION

### Selecting the Current-Sense Resistor ( $C_{CS}$ )

Choose the current-sense resistor ( $C_{CS}$ ) to be between 100mΩ and 300mΩ. If  $C_{CS}$  is too large, the CS voltage ( $V_{CS}$ ) can easily reach the OCP/shoot-through prevention threshold ( $V_{CS\_OCP}$ ), which can cause an early turn-off. If  $C_{CS}$  is too small, reaches the gate driver turn-on threshold ( $V_{CS\_ON}$ ) is not triggered in time. It is recommended that  $C_{CS}$  be 200mΩ.

### Selecting the Clamping Capacitor ( $C_{SN}$ )

The clamping capacitor ( $C_{SN}$ ) should be selected according to the leakage inductance ( $L_{LKG}$ ). The gate driver turn-on time (about 3/4 of the  $C_{SN}$  and  $L_{LKG}$  resonant period) should be shorter than the primary side's minimum turn-off time ( $t_{OFF\_MIN\_PRI}$ ).  $t_{OFF\_MIN\_PRI}$  can be calculated with Equation (2):

$$\frac{3}{2}\pi\sqrt{L_{LKG}C_{SN}} \leq t_{OFF\_MIN\_PRI} \quad (2)$$

$C_{SN}$  has a clamping effect on the drain-to-source voltage spike. Select a suitable  $C_{SN}$  to adjust the primary switch's voltage spike.

### Selecting the External MOSFET

Selecting the external MOSFET is a trade-off between the one resistance ( $R_{DS(ON)}$ ) and cost. For higher efficiency and improved thermal performance, a MOSFET with a smaller  $R_{DS(ON)}$  is recommended. However, MOSFETs with a smaller  $R_{DS(ON)}$  are typically more expensive. Additionally, MOSFETs with a body diode with a long reverse recovery time are recommended to facilitate the charge balance after the leakage inductance energy is recycled.

### Setting the Maximum Turn-on Time

The maximum turn-on time ( $t_{ON\_MAX}$ ) is set by an external resistor on the SET pin. It is recommended that  $t_{ON\_MAX}$  is slightly longer than the typical gate driver turn-on time.  $t_{ON\_MAX}$  can be calculated with Equation (3):

$$\frac{3}{2}\pi\sqrt{L_{LKG}C_{SN}} < t_{ON\_MAX} \quad (3)$$

Then  $t_{ON\_MAX}$  can guarantee that the gate driver turns off, even if  $V_{CS}$  does not reach the zero-current detection threshold ( $V_{CS\_ZCD}$ ) to prevent shoot-through.

The SET pin voltage ( $V_{SET}$ ) is susceptible to switching action that can lead to instability. It is recommended to connect a small capacitor across the SET pin's resistor ( $R_{SET}$ ) to filter out high-frequency noise.  $R_{SET}$  and its filter capacitor should be in a small package.

### PCB Layout Guidelines

Efficient PCB layout is critical for stable operation. For the best results, refer to Figure 5 and follow the guidelines below:

1. Place  $R_{SET}$  and its filter capacitor as close to the SET pin as possible.
2. Make the power loop and the sensing loop as small as possible.
3. Keep the IC out of the power loop to prevent the sensing loop and power loop from interrupting each other.
4. Place a ceramic decoupling capacitor from VDD to PGND close to the IC for adequate filtering.

### Layout Example

Figure 5 shows a double-layer PCB layout example. VSS is the primary main switch's drain side. BUS is the positive side of the BUS capacitor, R1 is the current-sense resistor, and C1 is the clamping capacitor.

1. Place  $R_{SET}$  and its filter capacitor (R3 and C3) as close to the SET pin as possible. In this example, R3 and C3 are in a 0402 package.

2. Minimize the power loop (VSS to R1 to M1 to C1 to BUS) and the sensing loop (CS to R1, and the VSS pin to the VSS side).
3. Separate the sensing loop from the power loop.
4. Place the VDD decoupling capacitor (C2) next to the VDD pin.
5. The VCC pin is connected to the primary controller's VCC through a diode (D1).

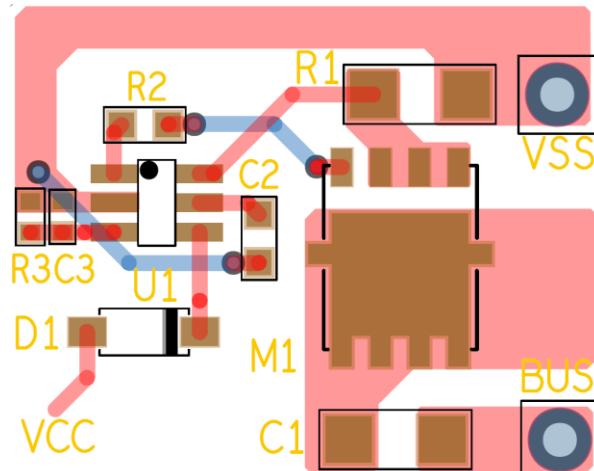
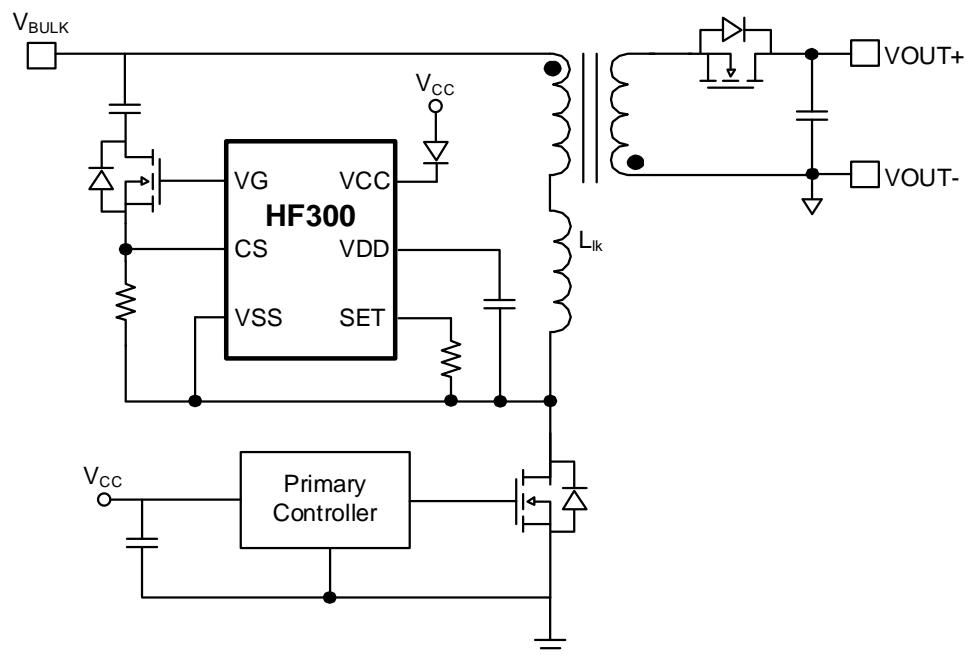
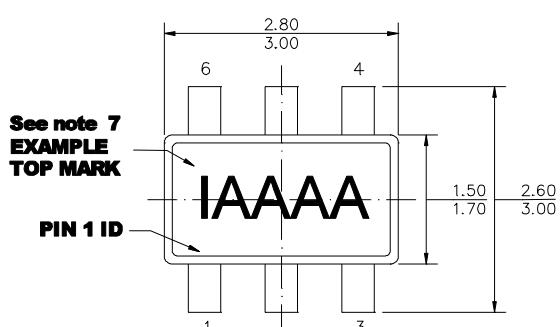


Figure 5: Recommended PCB Layout

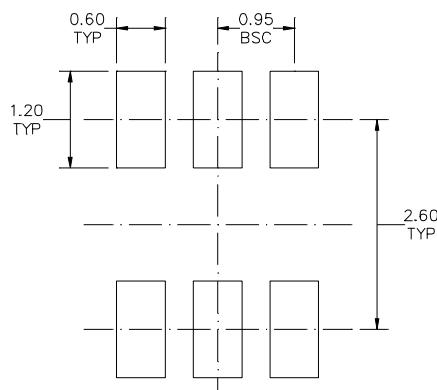
**TYPICAL APPLICATION CIRCUIT****Figure 6: Typical Application Circuit**

## PACKAGE INFORMATION

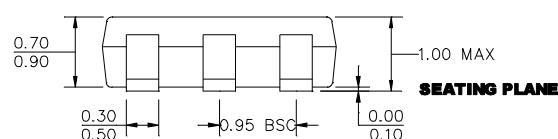
TSOT23-6



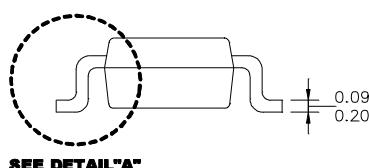
## TOP VIEW



## **RECOMMENDED LAND PATTERN**



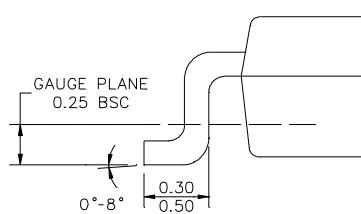
### FRONT VIEW



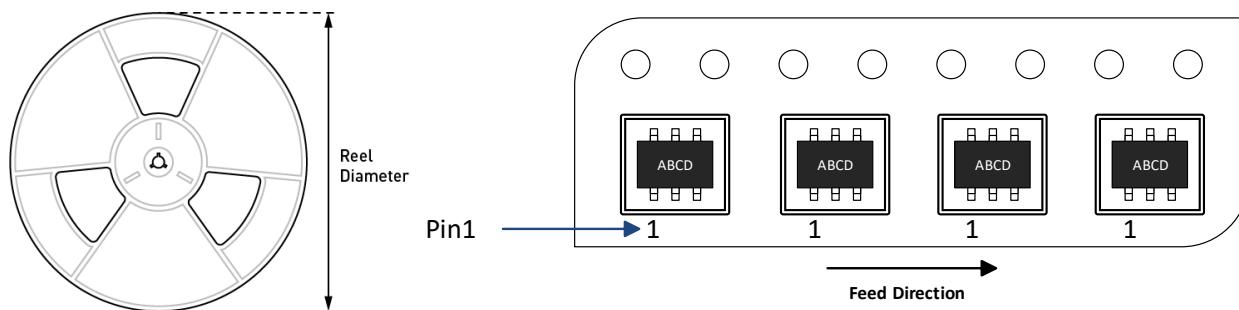
### SIDE VIEW

**NOTE:**

- 1) ALL DIMENSIONS ARE IN MILLIMETERS**
- 2) PACKAGE LENGTH DOES NOT INCLUDE MOLD FLASH  
PROTRUSION OR GATE BURR**
- 3) PACKAGE WIDTH DOES NOT INCLUDE INTERLEAD FLASH  
OR PROTRUSION**
- 4) LEAD COPLANARITY(BOTTOM OF LEADS AFTER FORMING  
SHALL BE 0.10 MILLIMETERS MAX**
- 5) DRAWING CONFORMS TO JEDEC MO193, VARIATION AB**
- 6) DRAWING IS NOT TO SCALE**
- 7) PIN 1 IS LOWER LEFT PIN WHEN READING TOP MARK  
FROM LEFT TO RIGHT, (SEE EXAMPLE TOP MARK)**



#### **DETAIL "A"**

**CARRIER INFORMATION**

Part Number	Package Description	Quantity/ Reel	Quantity/ Tube	Quantity/ Tray	Reel Diameter	Carrier Tape Width	Carrier Tape Pitch
HF300GJ-Z	TSOT23-6	3000	N/A	N/A	7in	8mm	4mm

**REVISION HISTORY**

<b>Revision #</b>	<b>Revision Date</b>	<b>Description</b>	<b>Pages Updated</b>
1.0	3/18/2024	Initial Release	-

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