



DESCRIPTION

The MP4323C is a configurable-frequency (350kHz to 2.5MHz), synchronous, step-down switching converter with integrated internal high-side and low-side power MOSFETs. The device provides 3A of highly efficient output current with peak current mode control.

The wide 3.3V to 36V input voltage range and 42V load dump tolerance accommodate a variety of step-down applications in automotive input environments. A 1µA shutdown mode quiescent current allows the device to be used in battery-powered applications.

The open-drain power good signal indicates when the output is within 94.5% to 105.5% of its nominal voltage.

Frequency foldback helps prevent inductor current runaway during start-up. Thermal shutdown provides reliable, fault-tolerant operation. A high duty cycle and low-dropout mode are provided for automotive cold-crank conditions.

The MP4323C is available in a QFN-14 (2.5mmx3.5mm) package.

FEATURES

- **Designed for Aftermarket Automotive Applications:**
 - Survives 42V Load Dump
 - Supports 3.1V Cold Crank
 - 3A of Continuous Output Current
 - Continuous Operation Up to 36V
 - Operating Junction Temperature from -40°C to +150°C
- **Increased Battery Life:**
 - 1µA Shutdown Supply Current
- **High Performance for Improved Thermals:**
 - Integrated 70mΩ High-Side MOSFET and 50mΩ Low-Side MOSFET
 - 65ns Minimum On Time and 50ns Minimum Off Time
- **Optimized for EMC/EMI:**
 - Frequency Spread Spectrum Modulation
 - Symmetric VIN Pinout
 - CISPR25 Class 5 Compliant
 - 350kHz to 2.5MHz Configurable Switching Frequency
 - MeshConnect™ Flip-Chip Package
- **Additional Features:**
 - Power Good Output
 - Forced Continuous Conduction Mode (FCCM)
 - Low-Dropout Mode
 - Hiccup Over-Current Protection (OCP)
 - Available in a QFN-14 (2.5mmx3.5mm) Package with Wettable Flanks

APPLICATIONS

- USB Chargers
- Aftermarket Automotive
- Battery-Powered Systems
- General Consumer Applications

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TYPICAL APPLICATION

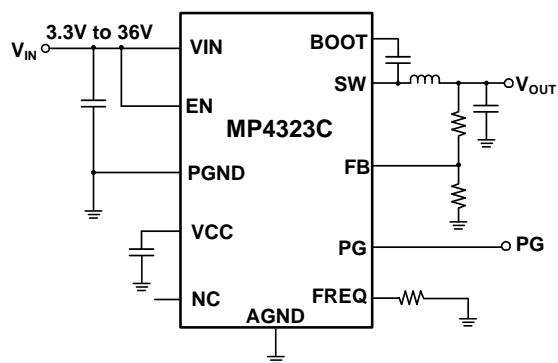


Figure 1: Typical Application (Adjustable Output)

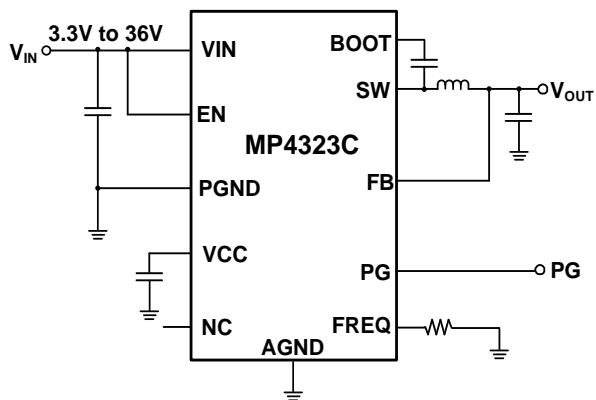
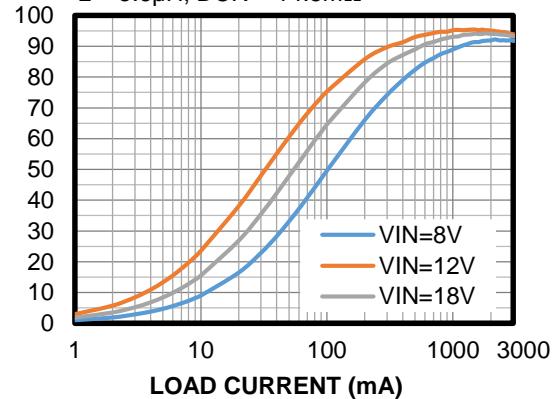


Figure 2: Typical Application (Fixed Output)

Efficiency vs. Load Current

$V_{OUT} = 5V$, $f_{SW} = 415\text{kHz}$,
 $L = 5.6\mu\text{H}$, $DCR = 14.5\text{m}\Omega$



ORDERING INFORMATION

Part Number ^{(1)*}	Package	Top Marking	MSL Rating ^{**}
MP4323CGRHE***	QFN-14 (2.5mmx3.5mm)	See Below	1

* For Tape & Reel, add suffix -Z (e.g. MP4323CGRHE-Z).

**Moisture Sensitivity Level Rating

***Wettable flank

Note:

1) Contact MPS for details on additional fixed output versions.

TOP MARKING

BTQ
YWW
LLL

BTQ: Production code of MP4323CGRHE

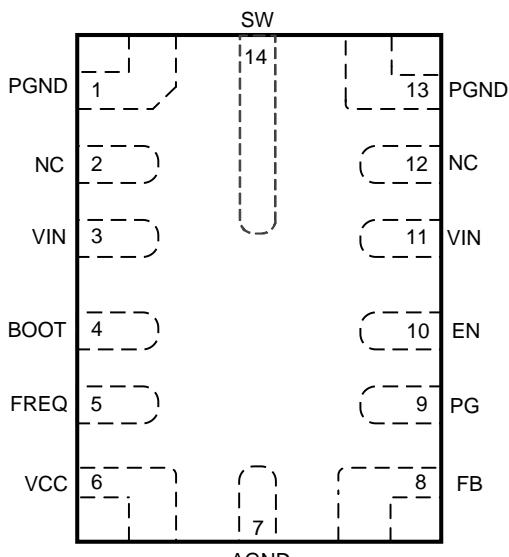
Y: Year code

WW: Week code

www.weakseed
111 : lot number

PACKAGE REFERENCE

TOP VIEW



QFN-14 (2.5mmx3.5mm)

PIN FUNCTIONS

Pin #	Name	Description
1, 13	PGND	Power ground.
2, 12	NC	No connection. The NC pins can be tied to GND.
3, 11	VIN	Input supply. VIN supplies power to all of the internal control circuitry, as well as the power switch connected to SW. The two VIN pins are connected internally. Connect a decoupling capacitor from VIN to ground (and close to each VIN pin) to minimize switching spikes.
4	BOOT	Bootstrap. BOOT is the positive power supply for the high-side MOSFET driver, which is connected to SW. Connect a bypass capacitor between BOOT and SW.
5	FREQ	Switching frequency configuration. Connect a resistor from FREQ to ground to set the switching frequency.
6	VCC	Biased supply. VCC is the output of the internal regulator that supplies power to the internal control circuit and gate drivers. Connect a minimum 1 μ F decoupling capacitor from VCC to ground, and place the capacitor as close as possible to the VCC pin.
7	AGND	Analog ground.
8	FB	Feedback input FB is the negative input of the error amplifier (typically 0.8V). For fixed output versions, connect this pin to the output voltage directly. For adjustable output versions, connect this pin to the middle point of the external feedback divider, between the output and AGND, to set the output voltage.
9	PG	Power good output. The output of PG is an open drain. If PG is used, it must be connected to the power source using a pull-up resistor. PG goes high if the output voltage is within 94.5% to 105.5% of the nominal voltage; PG goes low if the output voltage is above 107% or below 93% of the nominal voltage. Float PG if it is not used.
10	EN	Enable. Pull the EN pin below the specified threshold (about 0.85V) to shut down the chip. Pull EN above the specified threshold (about 1.02V) to enable the chip. The EN pin does not require an internal pull-up or pull-down resistor. Do not float the EN pin.
14	SW	Switch node. SW is the source of the high-side MOSFET, and the drain of the low-side MOSFET.

ABSOLUTE MAXIMUM RATINGS ⁽²⁾

VIN, EN.....	42V for automotive load dump ⁽³⁾
VIN, EN.....	-0.3V to 40V
SW.....	-0.3V to $V_{IN(MAX)} + 0.3V$
BOOT.....	$V_{SW} + 5.5V$
FREQ, VCC.....	5.5V
All other pins.....	-0.3V to +6V
Continuous power dissipation ($T_A = 25^\circ C$) ⁽⁴⁾	
QFN-14 (2.5mmx3.5mm)	3.7W ⁽⁸⁾
Operating junction temperature	+150°C
Lead temperature.....	+260°C
Storage temperature.....	-65°C to +150°C

ESD Ratings

Human body model (HBM)	Class 2 ⁽⁵⁾
Charged device model (CDM).....	Class C2b ⁽⁶⁾

Recommended Operating Conditions

Supply voltage (V_{IN}).....	3.3V to 36V
Minimum V_{IN} for start-up	3.9V
Minimum V_{IN} after start-up	3.1V
Output voltage (V_{OUT}).....	0.8V to $0.95 \times V_{IN}$
Operating junction temp (T_J)	
.....	-40°C to +150°C

Thermal Resistance θ_{JA} θ_{JC}

QFN-14 (2.5mmx3.5mm)	
JESD51-7.....	48.6.....7.4.....°C/W ⁽⁷⁾
EVQ4323C-RH-00A.....	33.6.....3.6.....°C/W ⁽⁸⁾

Notes:

- 2) Absolute maximum ratings are rated under room temperature, unless otherwise noted. Exceeding these ratings may damage the device.
- 3) Refer to ISO16750.
- 4) The maximum allowable power dissipation is a function of the maximum junction temperature, T_J (MAX), the junction-to-ambient thermal resistance, θ_{JA} , and the ambient temperature, T_A . The maximum allowable continuous power dissipation at any ambient temperature is calculated by P_D (MAX) = $(T_J$ (MAX) - T_A) / θ_{JA} . Exceeding the maximum allowable power dissipation can cause excessive die temperature, and the device may go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- 5) Per ANSI/ESDA/JEDEC JS-001.
- 6) Per ANSI/ESDA/JEDEC JS-002.
- 7) Measured on a JESD51-7, 4-layer PCB. The values given in this table are only valid for comparison with other packages and cannot be used for design purposes. These values were calculated in accordance with JESD51-7, and simulated on a specified JEDEC board. They do not represent the performance obtained in an actual application. The value of θ_{JC} shows the thermal resistance from junction-to-case bottom.
- 8) Measured on an MPS MP4323CGRHE standard EVB: 8.3cmx8.3cm, 2oz copper thickness, 4-layer PCB. The value of θ_{JC} shows the thermal resistance from junction-to-case top.

ELECTRICAL CHARACTERISTICS

$V_{IN} = 12V$, $V_{EN} = 2V$, $T_J = -40^{\circ}C$ to $+150^{\circ}C$ ⁽⁹⁾, typical values are at $T_J = 25^{\circ}C$, unless otherwise noted.

Parameter	Symbol	Condition	Min	Typ	Max	Units
Input Supply						
VIN under-voltage lockout rising threshold	$V_{IN\text{UVLO_RISING}}$		3.4	3.65	3.9	V
VIN under-voltage lockout falling threshold	$V_{IN\text{UVLO_FALLING}}$		2.6	2.9	3.1	V
VIN under-voltage lockout hysteresis	$V_{IN\text{UVLO_HYS}}$			750		mV
VIN active current (switching) ⁽¹⁰⁾	$I_{Q\text{_ACTIVE}}$	CCM, no load		1200		μA
VIN shutdown current	I_{SHDN}	$V_{EN} = 0V$		1	10	μA
VIN over-voltage protection rising threshold	$V_{IN\text{OVP_RISING}}$		35.5	37.5	40	V
VIN over-voltage protection falling threshold	$V_{IN\text{OVP_FALLING}}$		34.5	36.5	39	V
VIN over-voltage protection hysteresis	$V_{IN\text{OVP_HYS}}$			1		V
Switches and Frequency						
Switching frequency without frequency spread spectrum	f_{SW}	$R_{FREQ} = 86.6k\Omega$	332	415	498	kHz
		$R_{FREQ} = 34.8k\Omega$	900	1000	1100	kHz
		$R_{FREQ} = 15k\Omega$	1980	2200	2420	kHz
Frequency spread spectrum span				± 10		%
Frequency spread spectrum modulation frequency				15		kHz
Minimum on time ⁽¹⁰⁾	$t_{ON\text{_MIN}}$			65	80	ns
Minimum off time ⁽¹⁰⁾	$t_{OFF\text{_MIN}}$			50	70	ns
Maximum duty cycle	D_{MAX}		98	99.5		%
Switch leakage current	$I_{SW\text{_LKG}}$	$V_{EN} = 0V$, $V_{SW} = V_{BOOT} = 0V$ or V_{IN} ($T_J = 25^{\circ}C$)		0.01	1	μA
		$V_{EN} = 0V$, $V_{SW} = V_{BOOT} = 0V$ or V_{IN} ($T_J = -40^{\circ}C$ to $+150^{\circ}C$)		0.01	5	μA
HS switch on resistance	$R_{ON\text{_HS}}$	$V_{BOOT} - V_{SW} = 5V$		70	130	$m\Omega$
LS switch on resistance	$R_{ON\text{_LS}}$	$V_{CC} = 5V$		50	90	$m\Omega$

ELECTRICAL CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{EN} = 2V$, $T_J = -40^{\circ}C$ to $+150^{\circ}C$ ⁽⁹⁾, typical values are at $T_J = 25^{\circ}C$, unless otherwise noted.

Parameter	Symbol	Condition	Min	Typ	Max	Units
Output and Regulation						
FB voltage (adjustable output version)	V_{FB}	$T_J = 25^{\circ}C$	0.794	0.8	0.806	V
		$T_J = -40^{\circ}C$ to $+150^{\circ}C$	0.790	0.8	0.810	V
FB input current	I_{FB}	Adjustable output version		0	100	nA
V_{OUT} discharge current	$I_{DISCHARGE}$	$V_{EN} = 0V$, $V_{OUT} = 0.3V$	2	4		mA
BOOT						
BOOT - SW refresh rising	V_{BOOT_RISING}			2.5	2.9	V
BOOT - SW refresh falling	$V_{BOOT_FALLING}$			2.3	2.7	V
BOOT - SW refresh hysteresis	V_{BOOT_HYS}			0.2		V
EN						
EN rising threshold	V_{EN_RISING}		0.97	1.02	1.07	V
EN falling threshold	$V_{EN_FALLING}$		0.8	0.85	0.9	V
EN threshold hysteresis	V_{EN_HYS}			170		mV
Soft Start and VCC						
Soft-start time	t_{SS}	EN high to SS finishes	3	5	7	ms
VCC voltage	V_{CC}	$I_{VCC} = 0$	4.7	5	5.3	V
VCC regulation		$I_{VCC} = 30mA$		1		%
VCC current Limit	I_{LIMIT_VCC}	$V_{CC} = 4V$	50	70		mA
PG						
PG rising threshold (V_{FB} / V_{REF})	PG_{VTH_RISING}	V_{OUT} rising	93%	94.5%	96%	V_{REF}
		V_{OUT} falling	104%	105.5%	107%	
PG falling threshold (V_{FB} / V_{REF})	$PG_{VTH_FALLING}$	V_{OUT} falling	91.5%	93%	94.5%	
		V_{OUT} rising	105.5%	107%	108.5%	
PG threshold hysteresis (V_{FB} / V_{REF})	PG_{VTH_HYS}			1.5%		
PG output voltage low	V_{PG_LOW}	$I_{SINK} = 1mA$		0.1	0.3	V
PG rising deglitch time	t_{PG_R}			70		μs
PG falling deglitch time	t_{PG_F}			60		μs
Protections						
HS peak current limit	I_{LIMIT_HS}	Duty cycle = 30%	4.3	5.8	7.3	A
LS valley current limit	I_{LIMIT_LS}		3	4.4	5.7	A
LS reverse current limit	$I_{LIMIT_REVERSE}$			3		A
Thermal shutdown ⁽¹⁰⁾	T_{SD}		160	175	185	$^{\circ}C$
Thermal shutdown hysteresis ⁽¹⁰⁾	T_{SD_HYS}			20		$^{\circ}C$

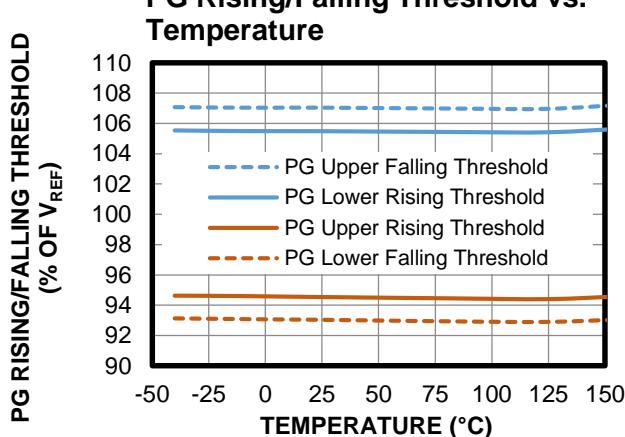
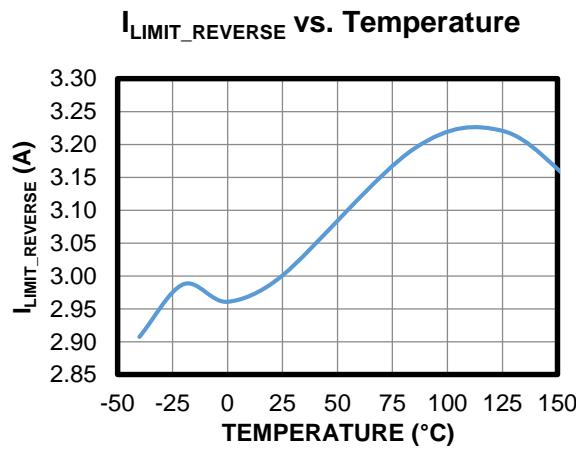
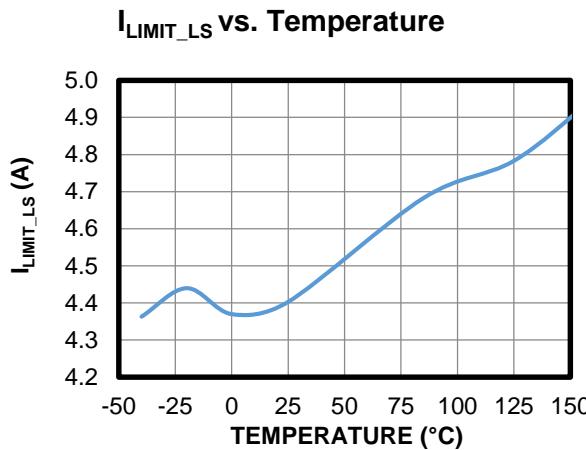
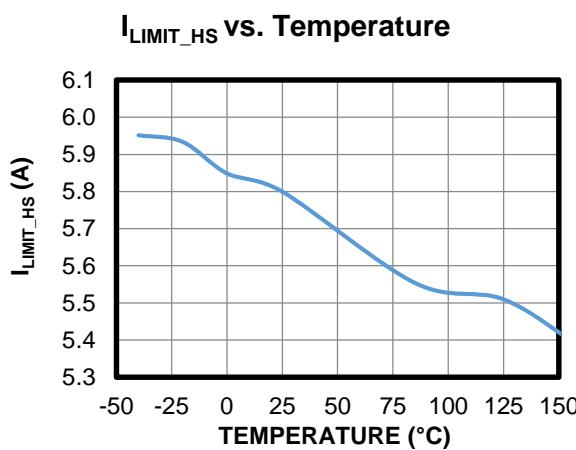
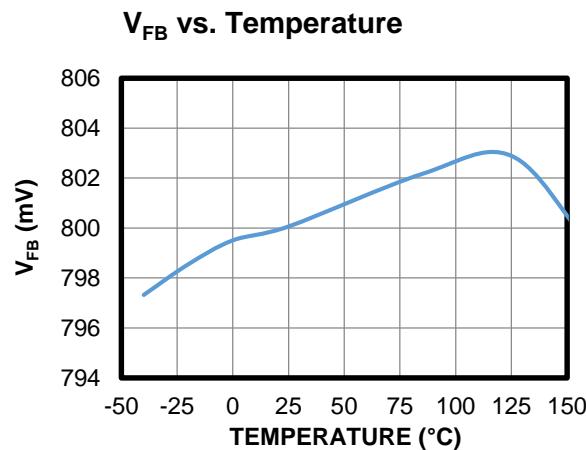
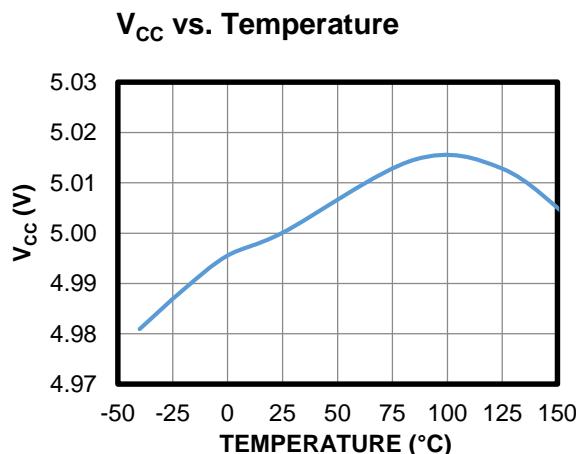
Notes:

9) Not tested in production. Guaranteed by over temperature correlation.

10) Not tested in production. Guaranteed by design and characterization.

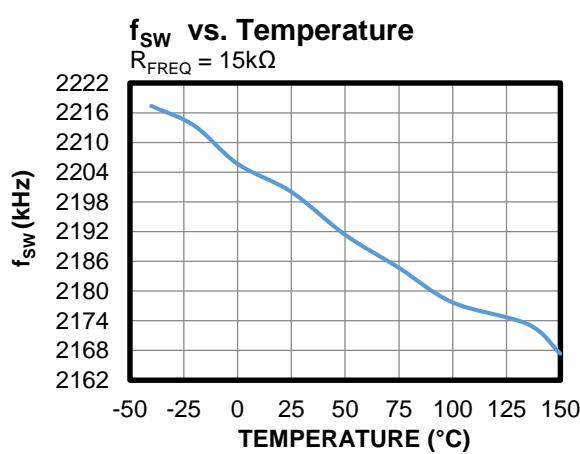
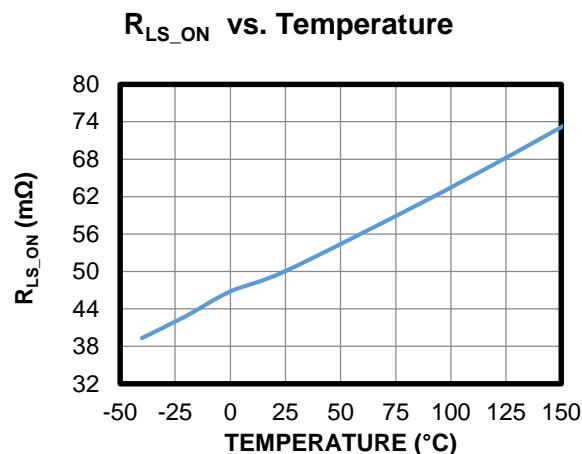
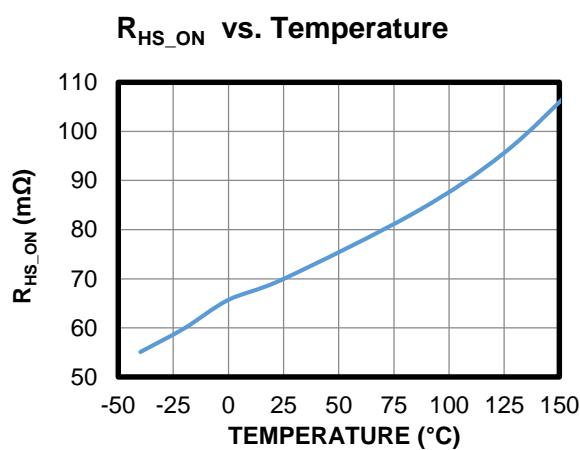
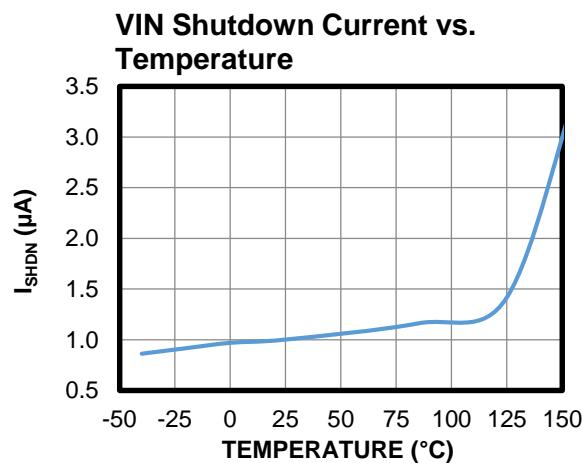
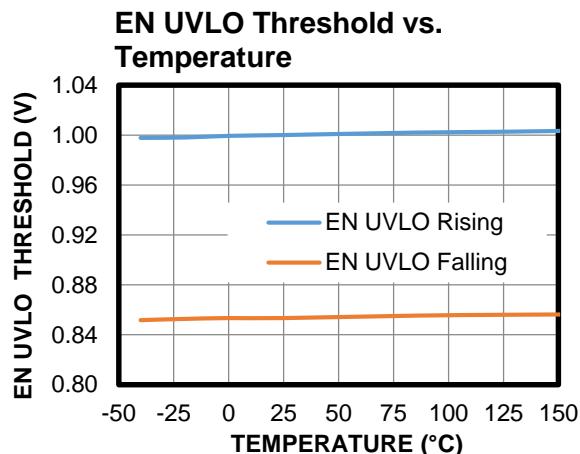
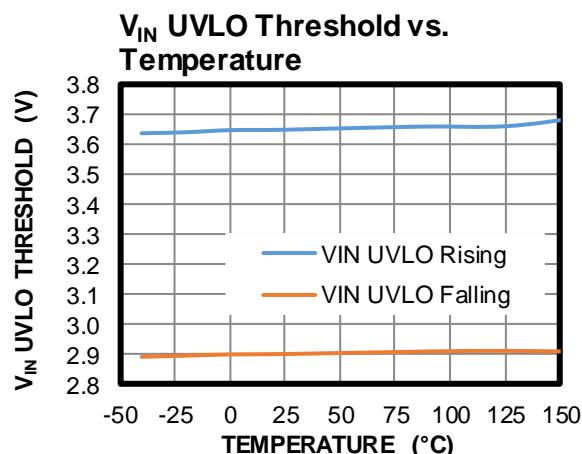
TYPICAL CHARACTERISTICS

V_{IN} = 12V, unless otherwise noted.



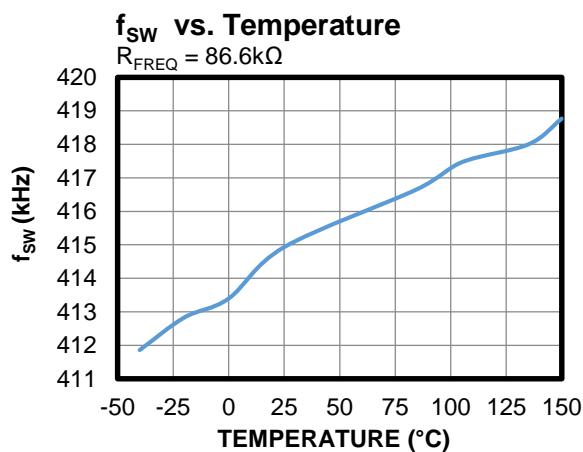
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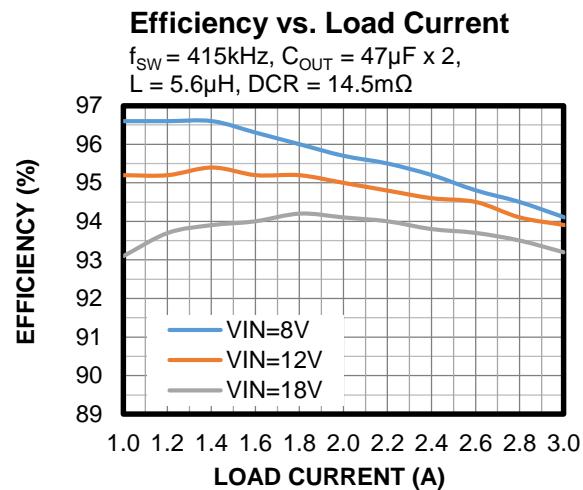
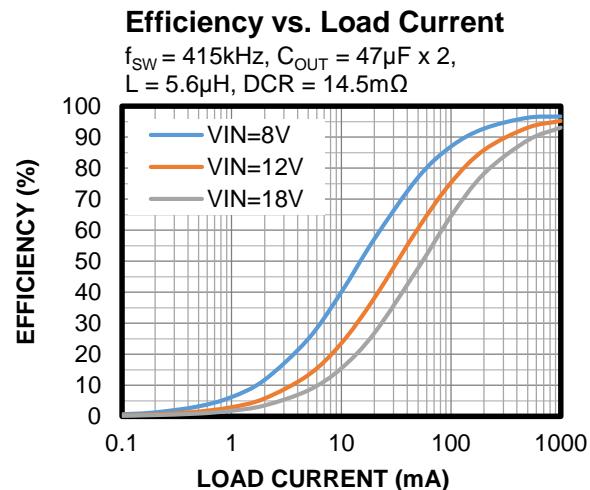
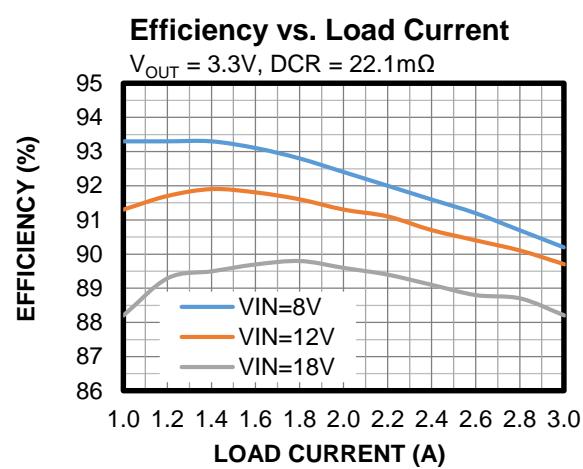
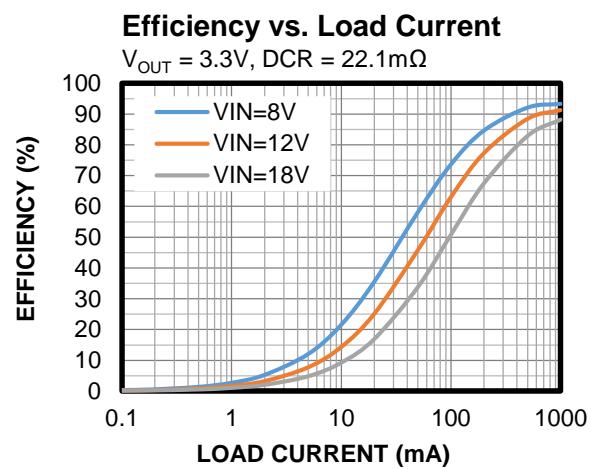
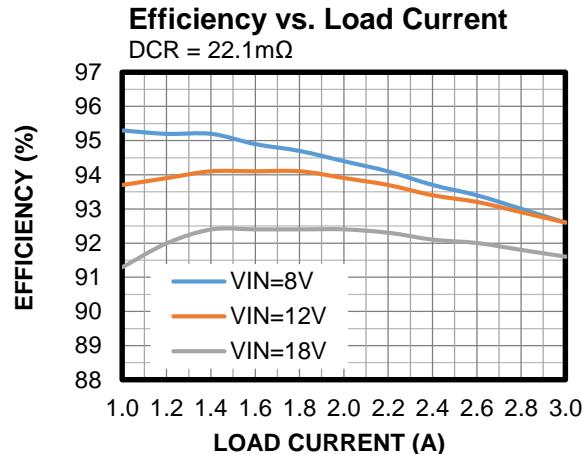
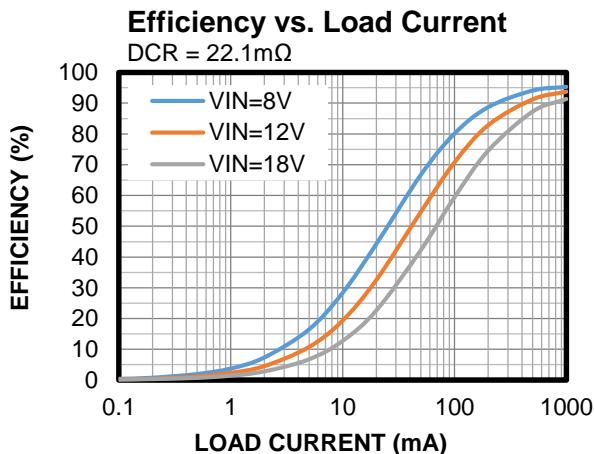
TYPICAL CHARACTERISTICS (continued)

V_{IN} = 12V, unless otherwise noted.



TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{SW} = 2.2MHz$, $L = 2.2\mu H$, $C_{OUT} = 22\mu F \times 2$, $T_A = 25^\circ C$, unless otherwise noted.

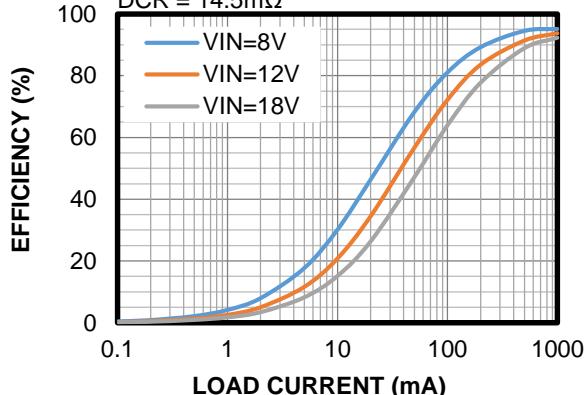


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{SW} = 2.2MHz$, $L = 2.2\mu H$, $C_{OUT} = 22\mu F \times 2$, $T_A = 25^\circ C$, unless otherwise noted.

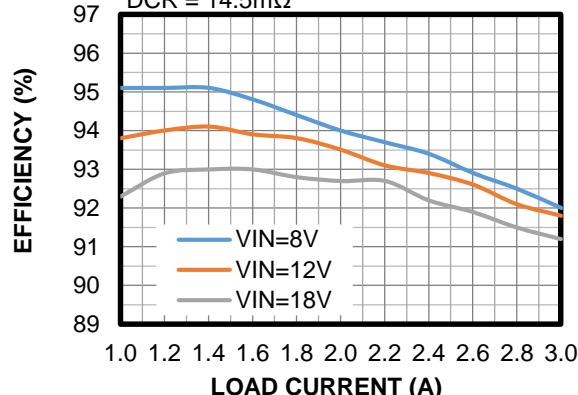
Efficiency vs. Load Current

$V_{OUT} = 3.3V$, $f_{SW} = 415kHz$,
 $C_{OUT} = 47\mu F \times 2$, $L = 5.6\mu H$,
 $DCR = 14.5m\Omega$



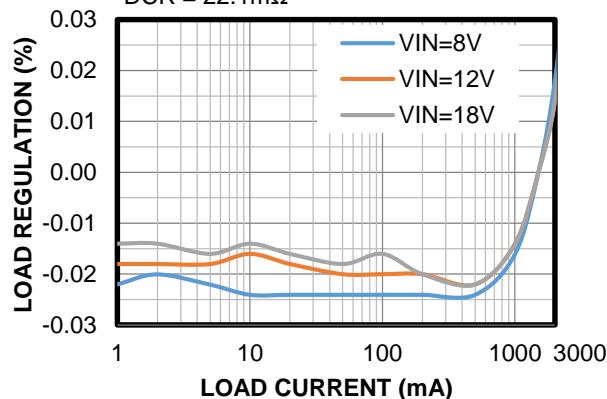
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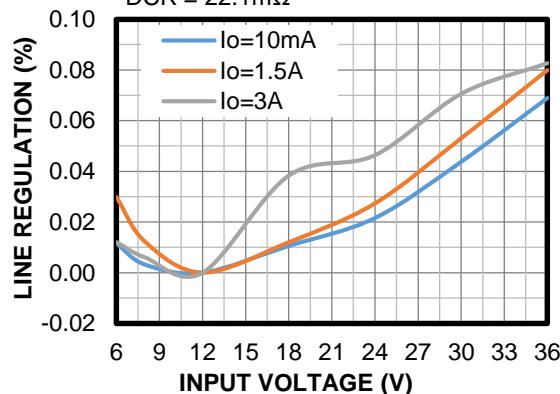
Load Regulation

$DCR = 22.1m\Omega$



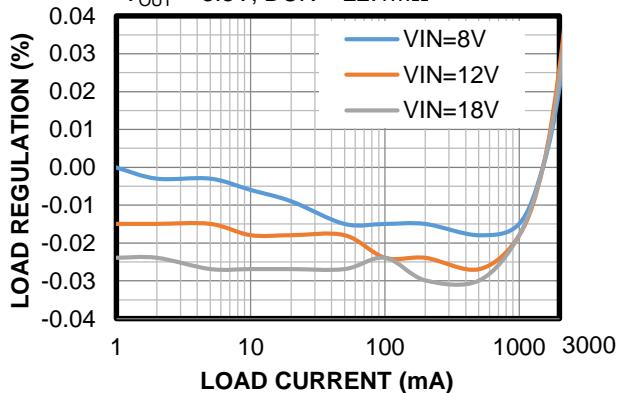
Line Regulation

$DCR = 22.1m\Omega$



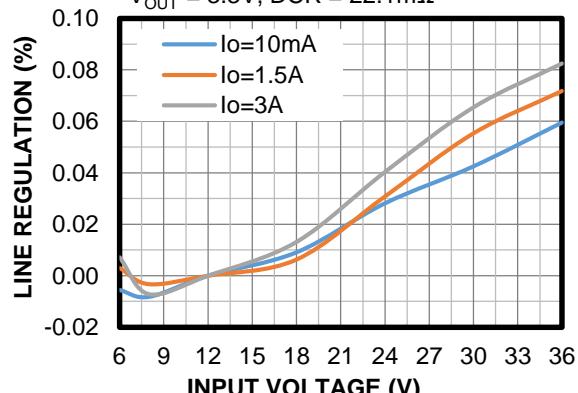
Load Regulation

$V_{OUT} = 3.3V$, $DCR = 22.1m\Omega$



Line Regulation

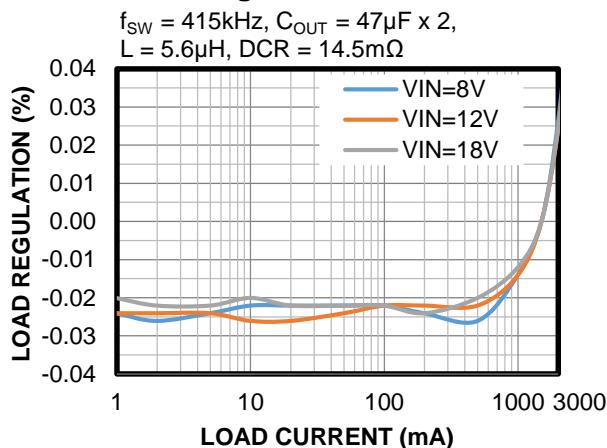
$V_{OUT} = 3.3V$, $DCR = 22.1m\Omega$



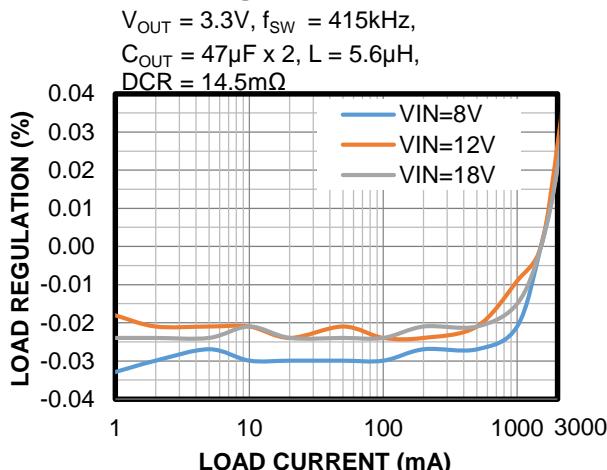
TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{SW} = 2.2MHz$, $L = 2.2\mu H$, $C_{OUT} = 22\mu F \times 2$, $T_A = 25^\circ C$, unless otherwise noted.

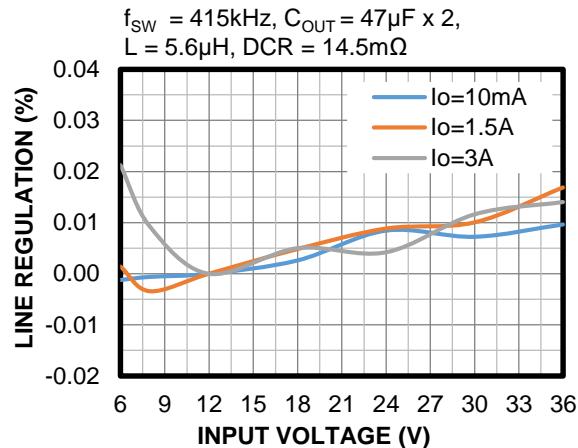
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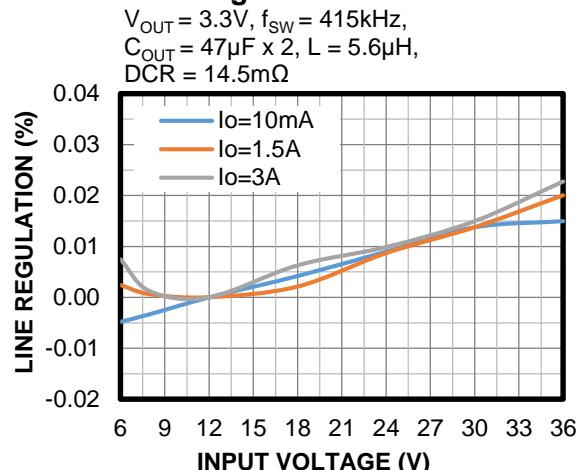
Load Regulation



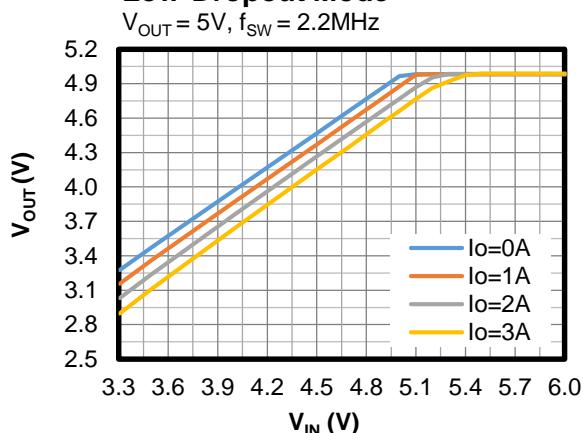
Line Regulation



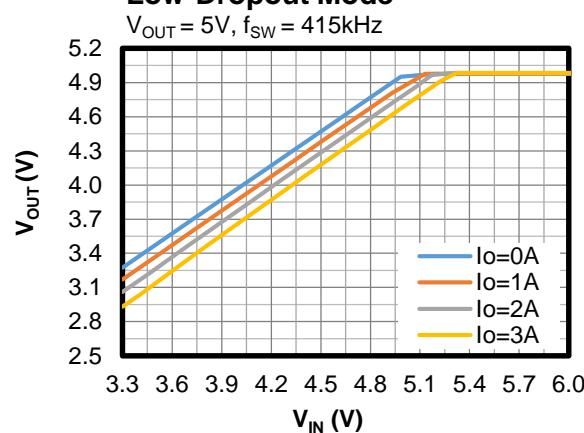
Line Regulation



Low-Dropout Mode

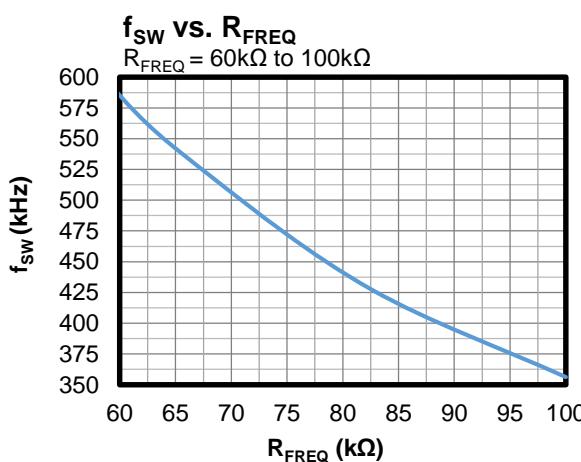
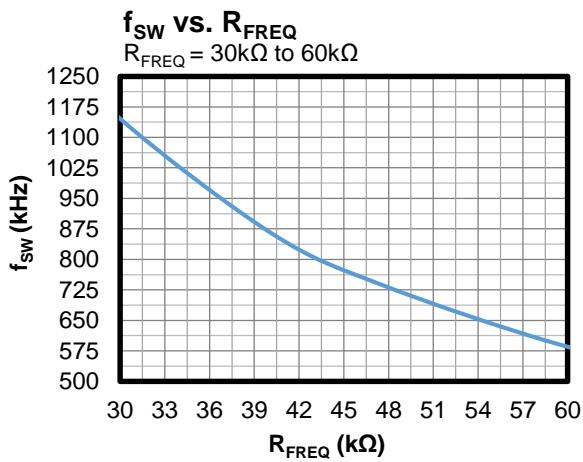
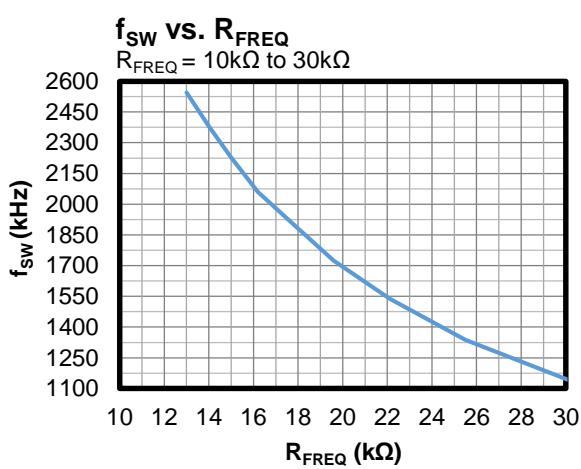
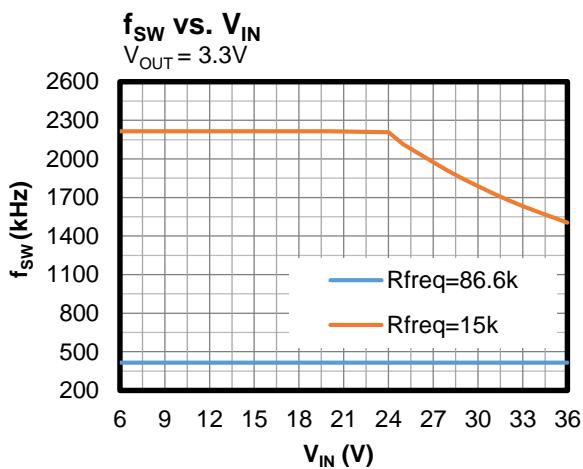
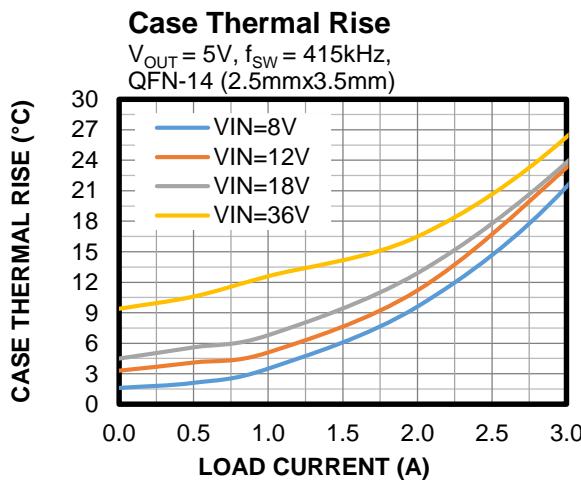
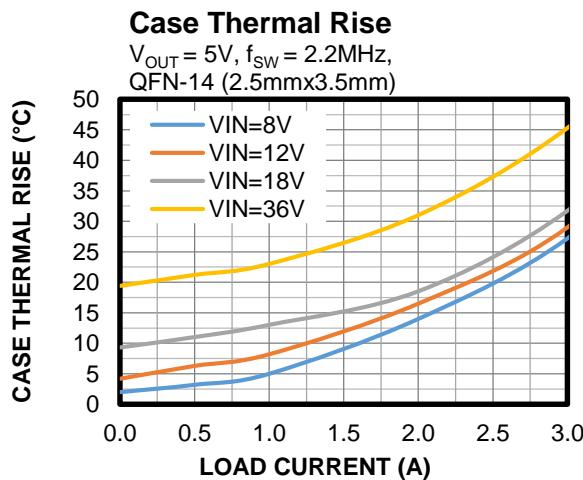


Low-Dropout Mode



TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{SW} = 2.2\text{MHz}$, $L = 2.2\mu\text{H}$, $C_{OUT} = 22\mu\text{F} \times 2$, $T_A = 25^\circ\text{C}$, unless otherwise noted.

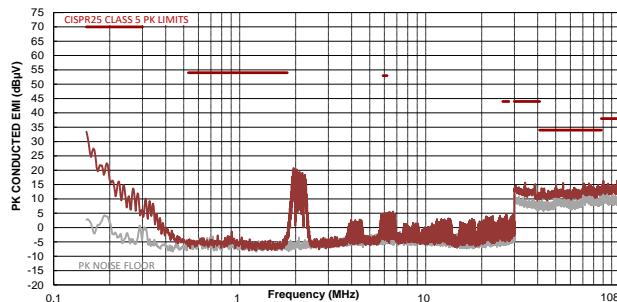


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{SW} = 2.2\text{MHz}$, $L = 2.2\mu\text{H}$, $C_{OUT} = 22\mu\text{F} \times 2$, $T_A = 25^\circ\text{C}$, unless otherwise noted.⁽¹¹⁾

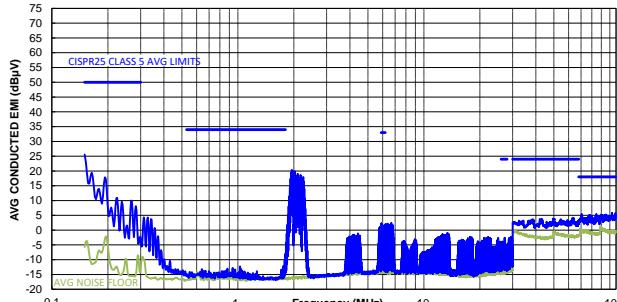
CISPR25 Class 5 Peak Conducted Emissions

150kHz to 108MHz



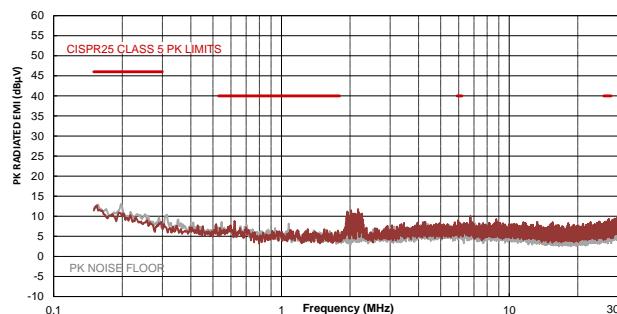
CISPR25 Class 5 Average Conducted Emissions

150kHz to 108MHz



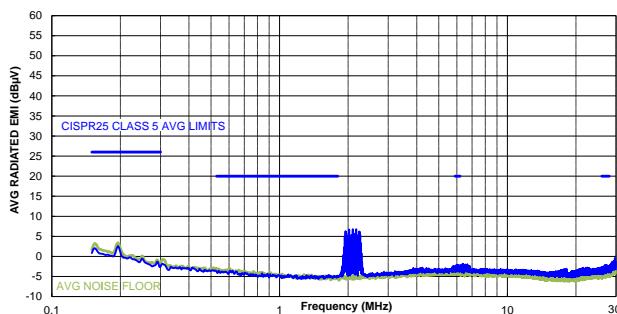
CISPR25 Class 5 Peak Radiated Emissions

150kHz to 30MHz



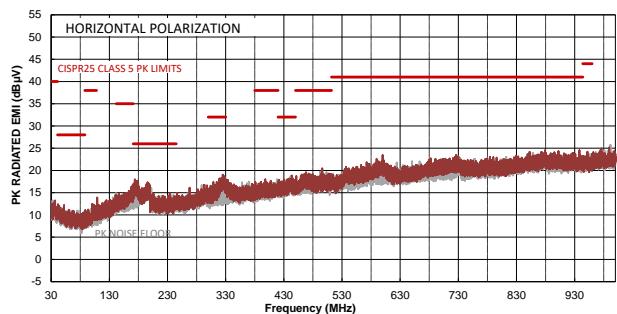
CISPR25 Class 5 Average Radiated Emissions

150kHz to 30MHz



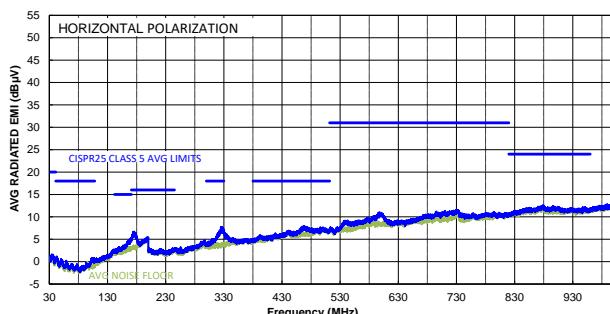
CISPR25 Class 5 Peak Radiated Emissions

Horizontal, 30MHz to 1GHz



CISPR25 Class 5 Average Radiated Emissions

Horizontal, 30MHz to 1GHz

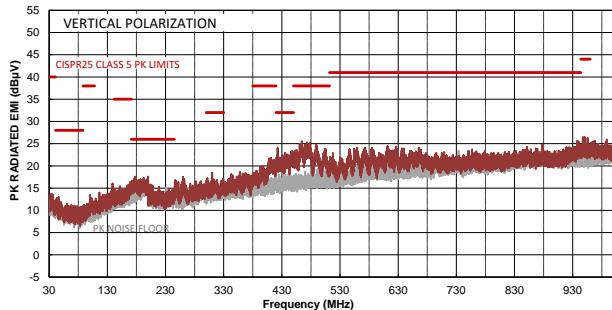


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{SW} = 2.2\text{MHz}$, $L = 2.2\mu\text{H}$, $C_{OUT} = 22\mu\text{F} \times 2$, $T_A = 25^\circ\text{C}$, unless otherwise noted.⁽¹¹⁾

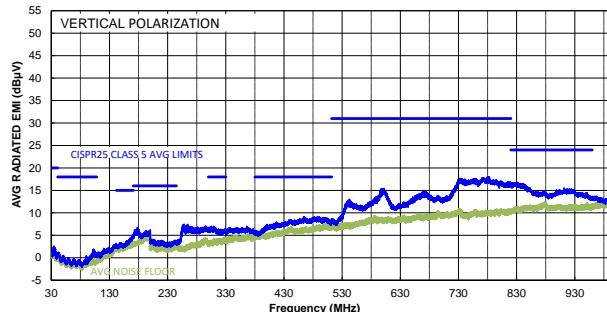
CISPR25 Class 5 Peak Radiated Emissions

Vertical, 30MHz to 1GHz



CISPR25 Class 5 Average Radiated Emissions

Vertical, 30MHz to 1GHz



Note:

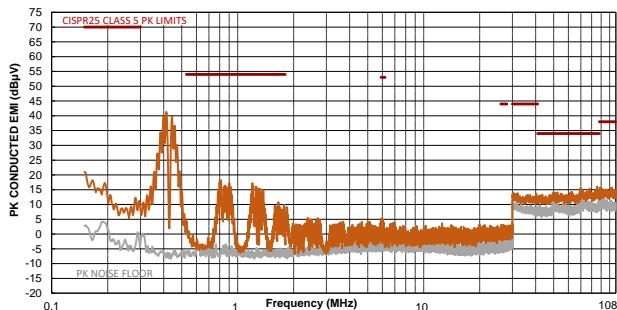
11) The EMC test results are based on the application circuit with EMI filters (see Figure 15 on page 36).

TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{SW} = 415\text{kHz}$, $L = 5.6\mu\text{H}$, $C_{OUT} = 47\mu\text{F} \times 2$, $T_A = 25^\circ\text{C}$, unless otherwise noted.⁽¹²⁾

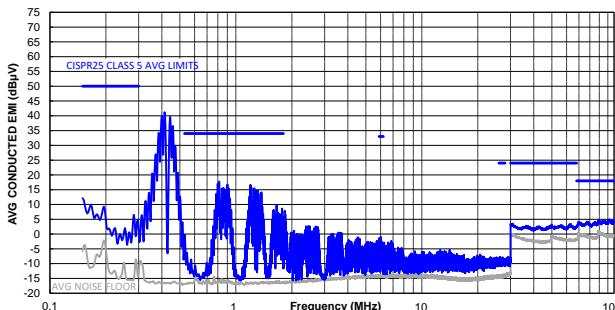
CISPR25 Class 5 Peak Conducted Emissions

150kHz to 108MHz



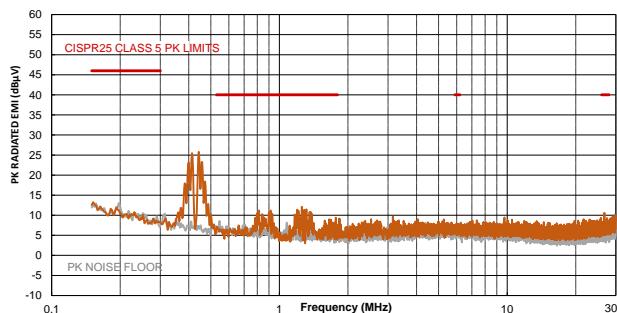
CISPR25 Class 5 Average Conducted Emissions

150kHz to 108MHz



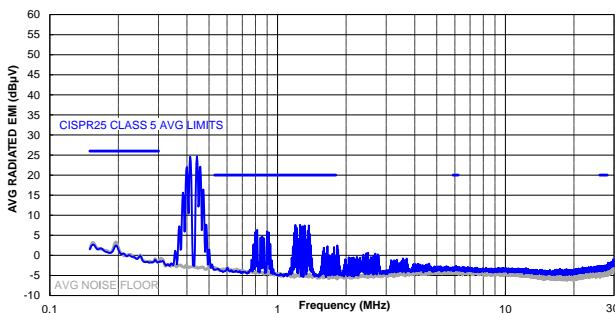
CISPR25 Class 5 Peak Radiated Emissions

150kHz to 30MHz



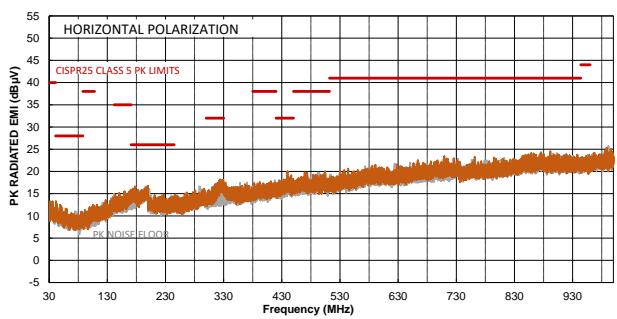
CISPR25 Class 5 Average Radiated Emissions

150kHz to 30MHz



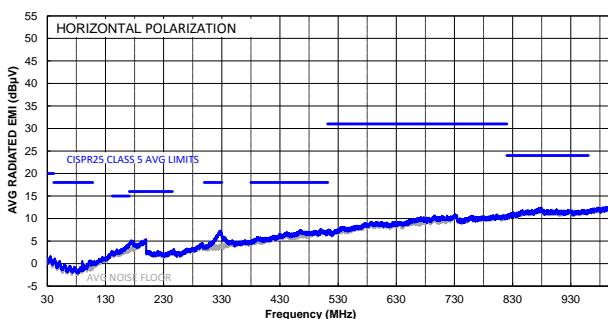
CISPR25 Class 5 Peak Radiated Emissions

Horizontal, 30MHz to 1GHz



CISPR25 Class 5 Average Radiated Emissions

Horizontal, 30MHz to 1GHz

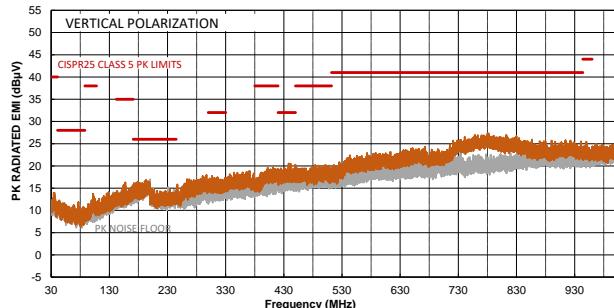


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

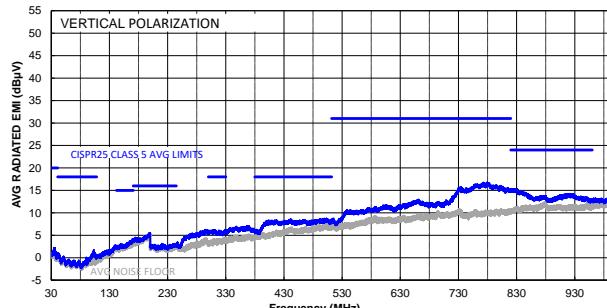
$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{SW} = 415\text{kHz}$, $L = 5.6\mu\text{H}$, $C_{OUT} = 47\mu\text{F} \times 2$, $T_A = 25^\circ\text{C}$, unless otherwise noted.⁽¹²⁾

CISPR25 Class 5 Peak Radiated Emissions

Vertical, 30MHz to 1GHz

**CISPR25 Class 5 Average Radiated Emissions**

Vertical, 30MHz to 1GHz

**Note:**

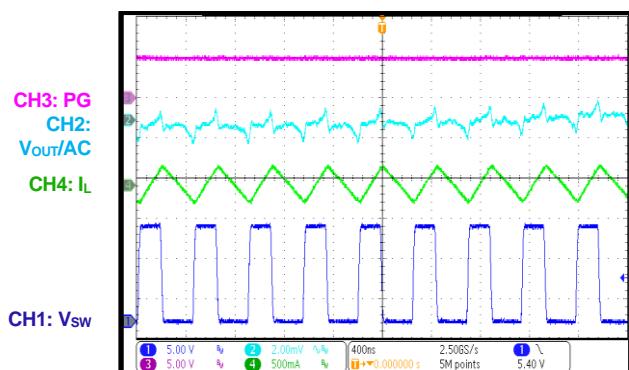
12) The EMC test results are based on the application circuit with EMI filters (see Figure 16 on page 37).

TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{sw} = 2.2MHz$, $L = 2.2\mu H$, $C_{OUT} = 22\mu F \times 2$, $T_A = 25^{\circ}C$, unless otherwise noted.

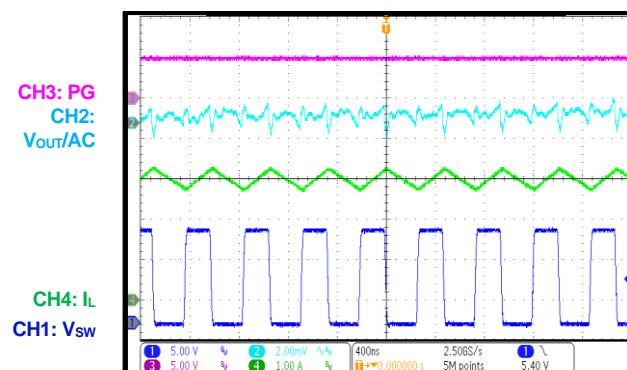
Steady State

$I_{OUT} = 0A$



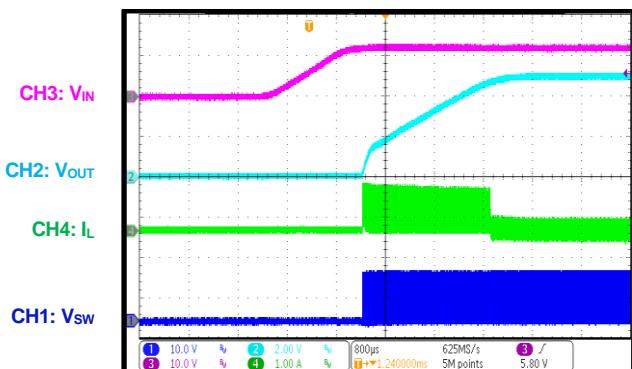
Steady State

$I_{OUT} = 3A$



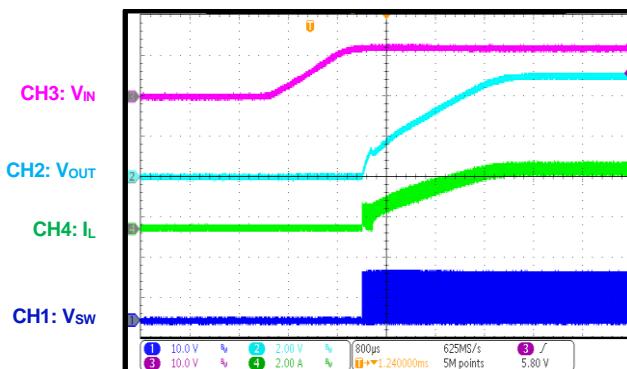
Start-Up through VIN

$I_{OUT} = 0A$



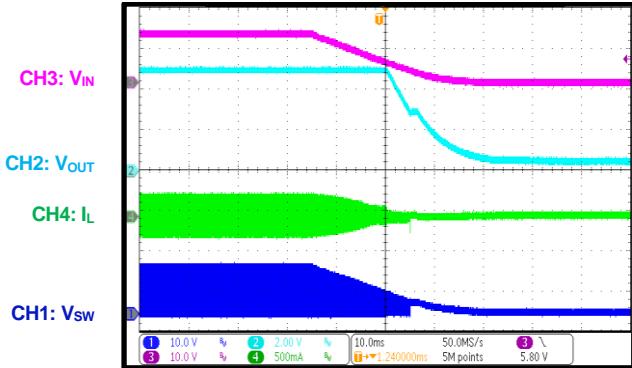
Start-Up through VIN

$I_{OUT} = 3A$



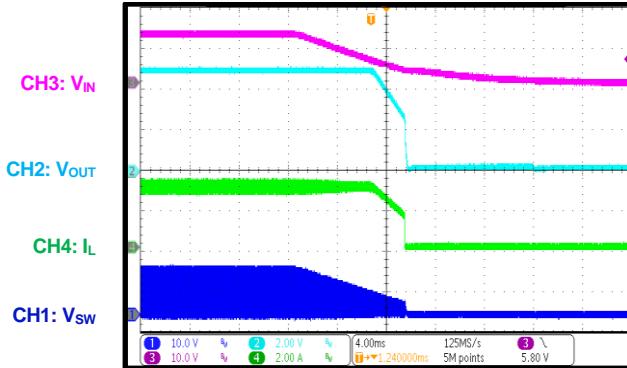
Shutdown through VIN

$I_{OUT} = 0A$



Shutdown through VIN

$I_{OUT} = 3A$

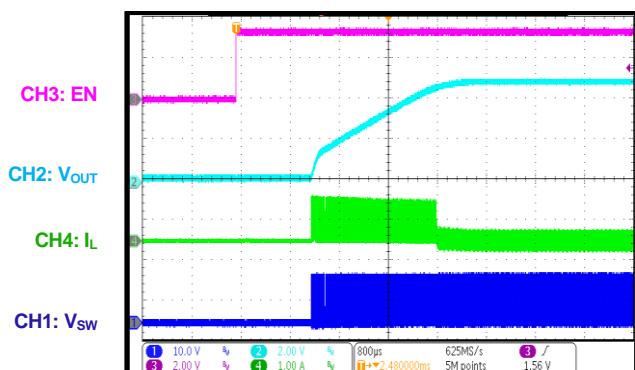


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{SW} = 2.2MHz$, $L = 2.2\mu H$, $C_{OUT} = 22\mu F \times 2$, $T_A = 25^\circ C$, unless otherwise noted.

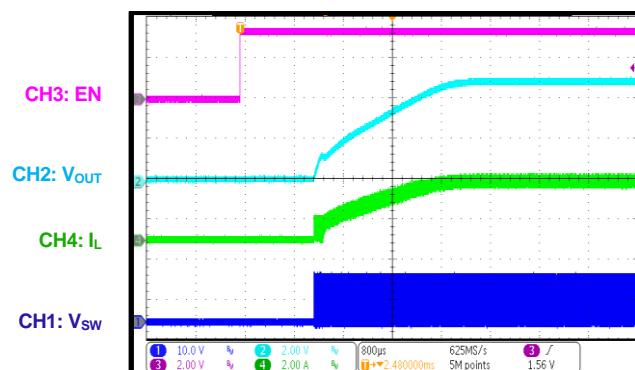
Start-Up through EN

$I_{OUT} = 0A$



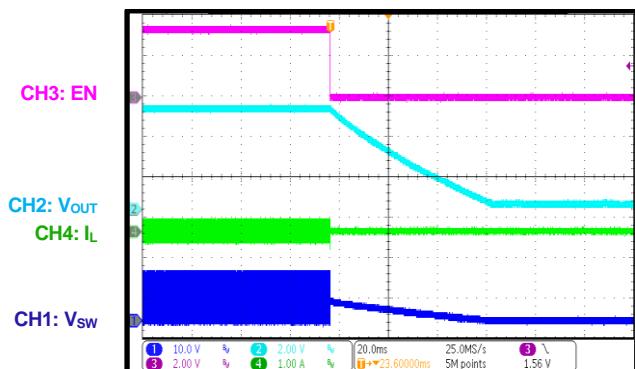
Start-Up through EN

$I_{OUT} = 3A$



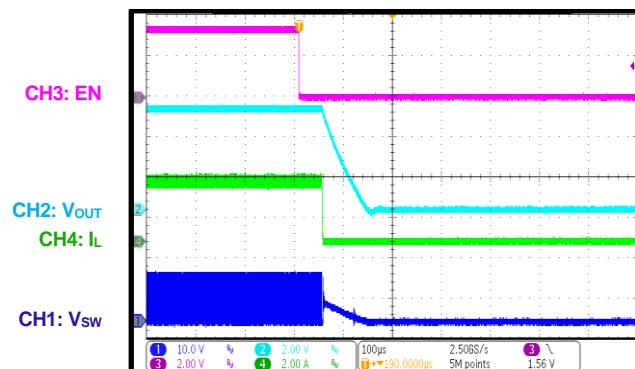
Shutdown through EN

$I_{OUT} = 0A$



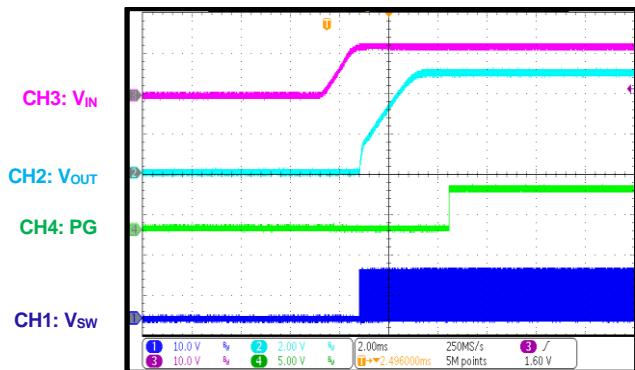
Shutdown through EN

$I_{OUT} = 3A$



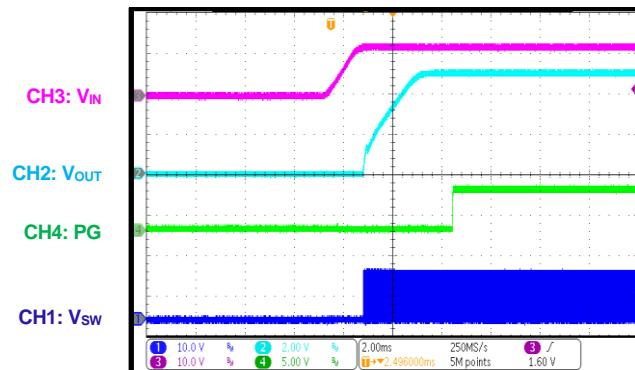
PG in Start-Up through VIN

$I_{OUT} = 0A$



PG in Start-Up through VIN

$I_{OUT} = 3A$

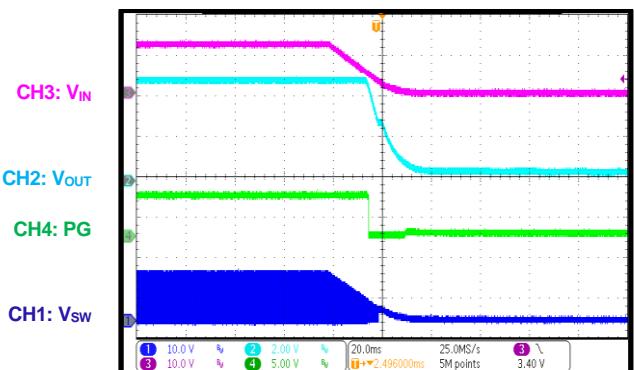


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

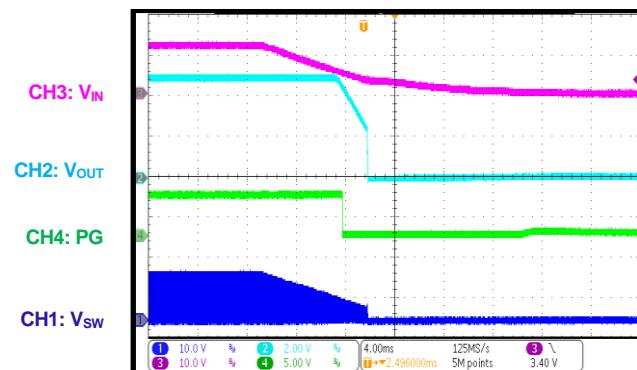
$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{sw} = 2.2MHz$, $L = 2.2\mu H$, $C_{OUT} = 22\mu F \times 2$, $T_A = 25^\circ C$, unless otherwise noted.

PG in Shutdown through VIN

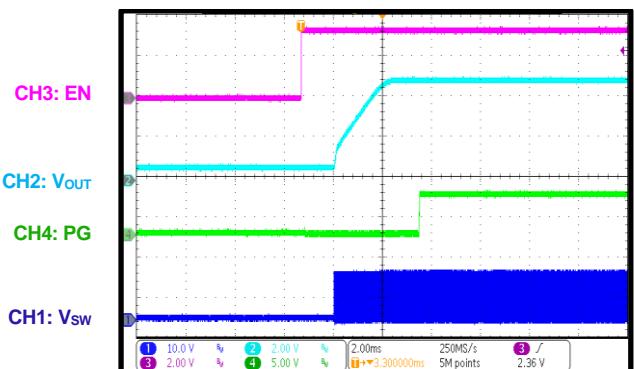
$I_{OUT} = 0A$


PG in Shutdown through VIN

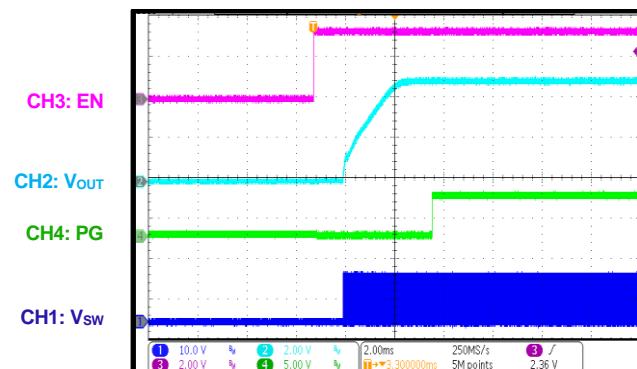
$I_{OUT} = 3A$


PG in Start-Up through EN

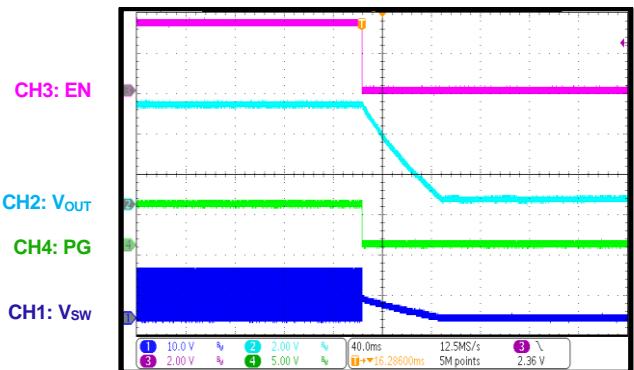
$I_{OUT} = 0A$


PG in Start-Up through EN

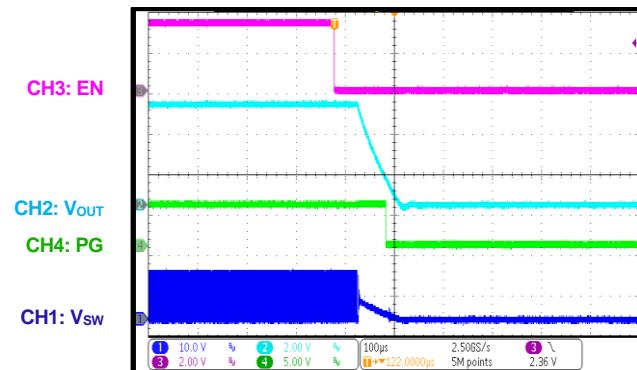
$I_{OUT} = 3A$


PG in Shutdown through EN

$I_{OUT} = 0A$


PG in Shutdown through EN

$I_{OUT} = 3A$

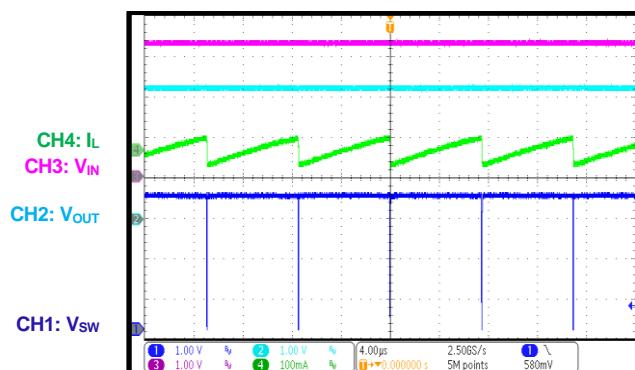


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{SW} = 2.2MHz$, $L = 2.2\mu H$, $C_{OUT} = 22\mu F \times 2$, $T_A = 25^\circ C$, unless otherwise noted.

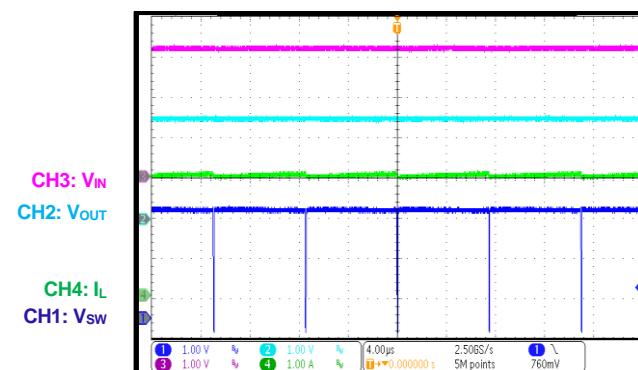
Low-Dropout Mode

$I_{OUT} = 0A$, $V_{IN} = 3.3V$



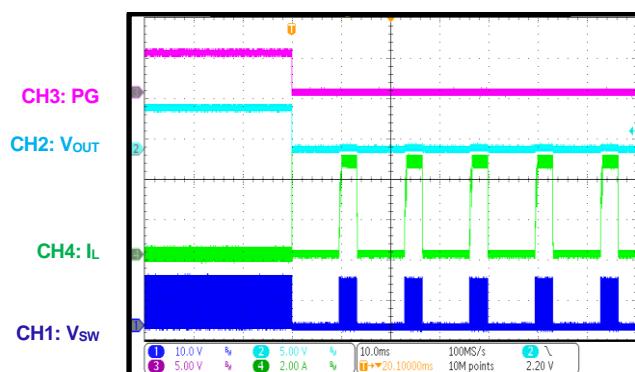
Low-Dropout Mode

$I_{OUT} = 3A$, $V_{IN} = 3.3V$



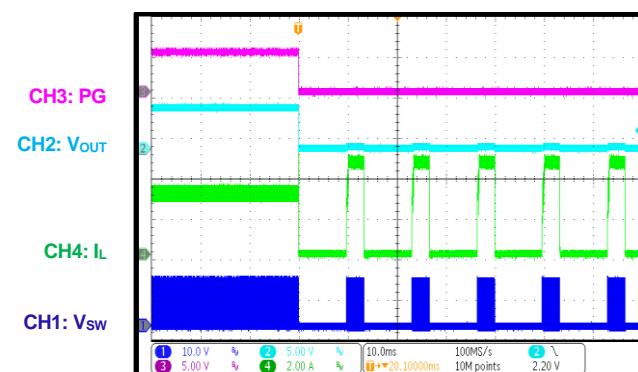
SCP Entry

$I_{OUT} = 0A$



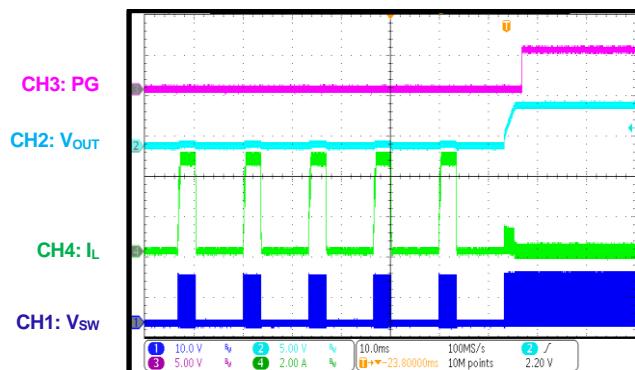
SCP Entry

$I_{OUT} = 3A$



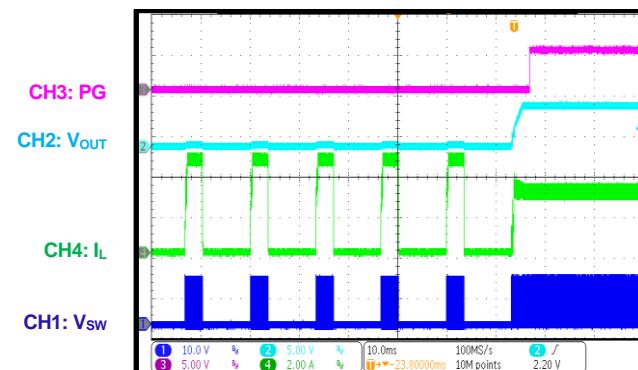
SCP Recovery

$I_{OUT} = 0A$



SCP Recovery

$I_{OUT} = 3A$

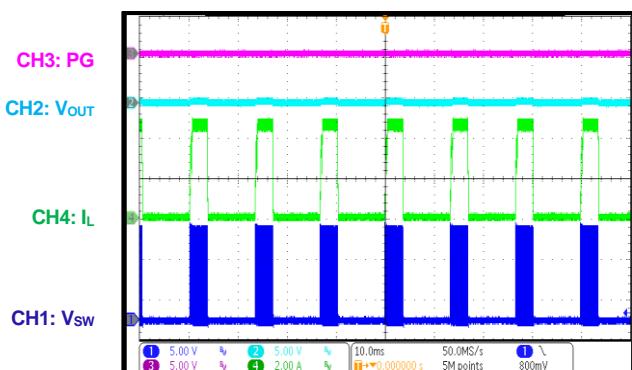


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{SW} = 2.2MHz$, $L = 2.2\mu H$, $C_{OUT} = 22\mu F \times 2$, $T_A = 25^\circ C$, unless otherwise noted.

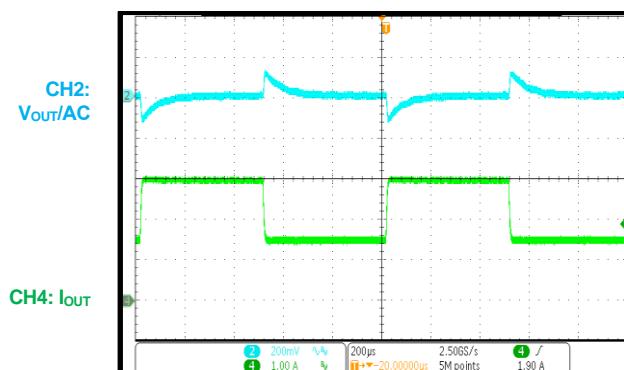
SCP Steady State

$I_{OUT} = 0A$



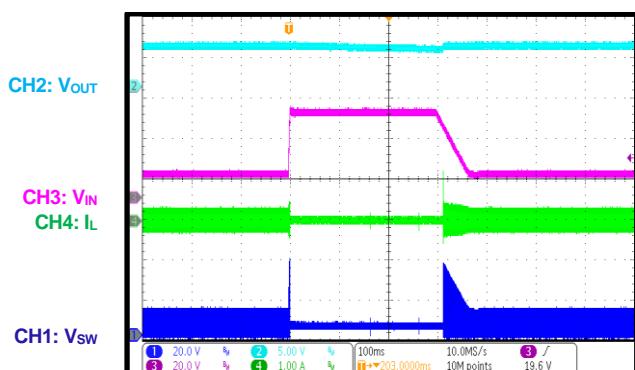
Load Transient

$I_{OUT} = 1.5A$ to $3A$, $1.6A/\mu s$



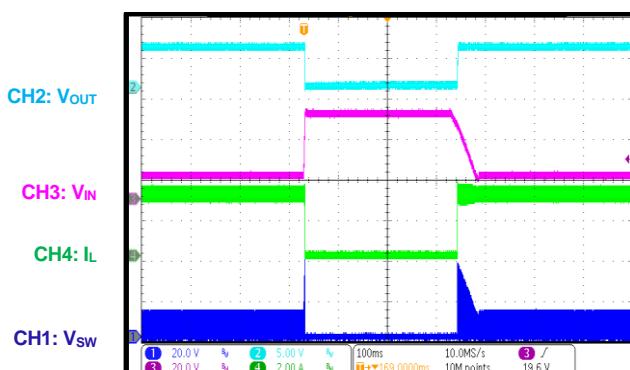
Load Dump

$V_{IN} = 12V$ to $42V$, $I_{OUT} = 0A$



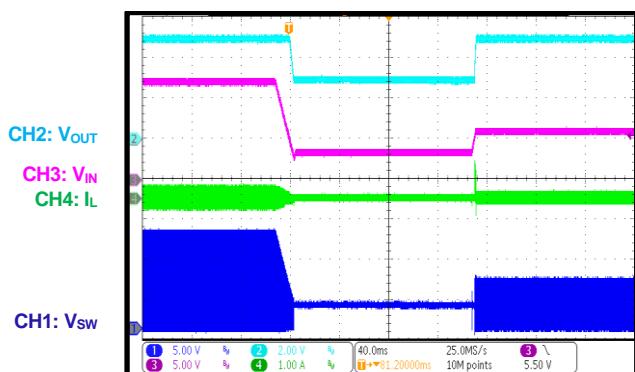
Load Dump

$V_{IN} = 12V$ to $42V$, $I_{OUT} = 3A$



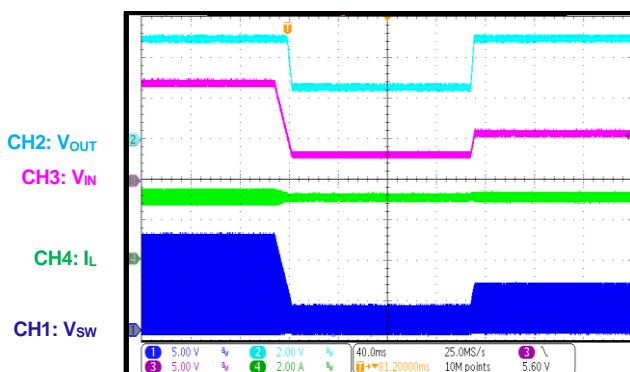
Cold Crank

$V_{IN} = 12V$ to $3.3V$ to $6V$, $I_{OUT} = 0A$



Cold Crank

$V_{IN} = 12V$ to $3.3V$ to $6V$, $I_{OUT} = 3A$

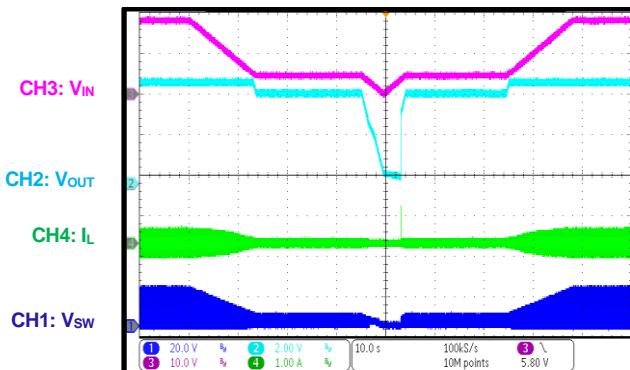


TYPICAL PERFORMANCE CHARACTERISTICS (continued)

$V_{IN} = 12V$, $V_{OUT} = 5V$, $f_{SW} = 2.2MHz$, $L = 2.2\mu H$, $C_{OUT} = 22\mu F \times 2$, $T_A = 25^\circ C$, unless otherwise noted.

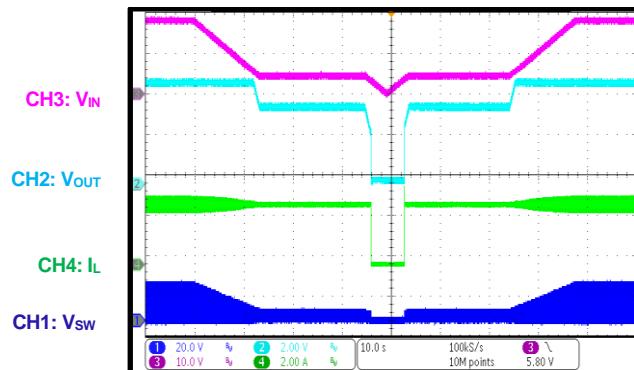
VIN Ramp Down and Up

$V_{IN} = 18V$ to $4.5V$ to $0V$ to $4.5V$ to $18V$, $I_{OUT} = 0A$



VIN Ramp Down and Up

$V_{IN} = 18V$ to $4.5V$ to $0V$ to $4.5V$ to $18V$, $I_{OUT} = 3A$



FUNCTIONAL BLOCK DIAGRAM

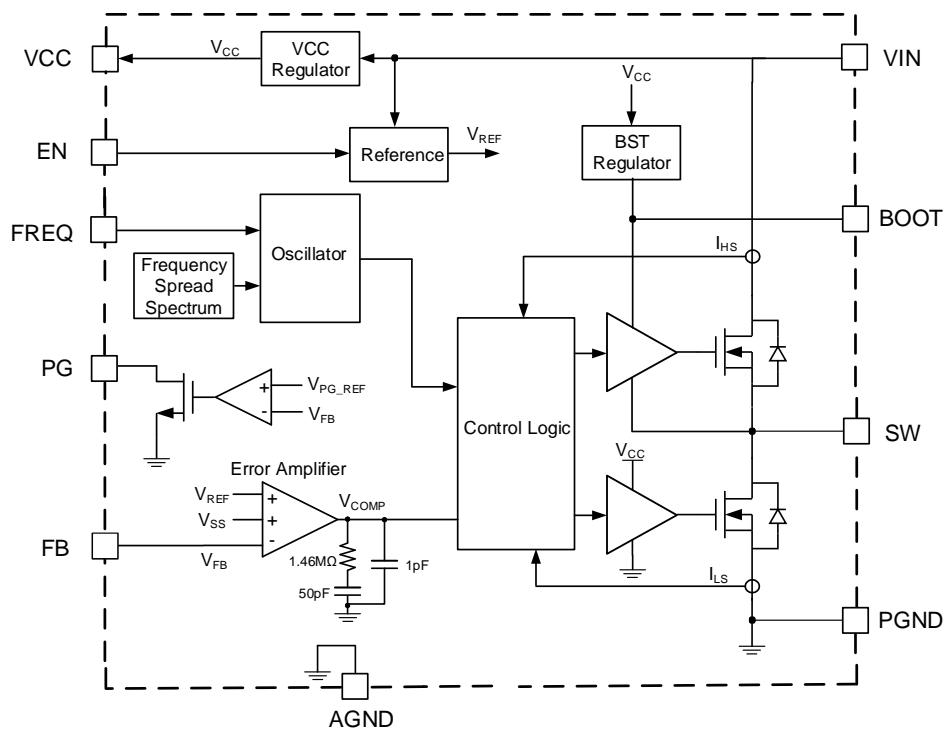


Figure 3: Functional Block Diagram (Adjustable Output)

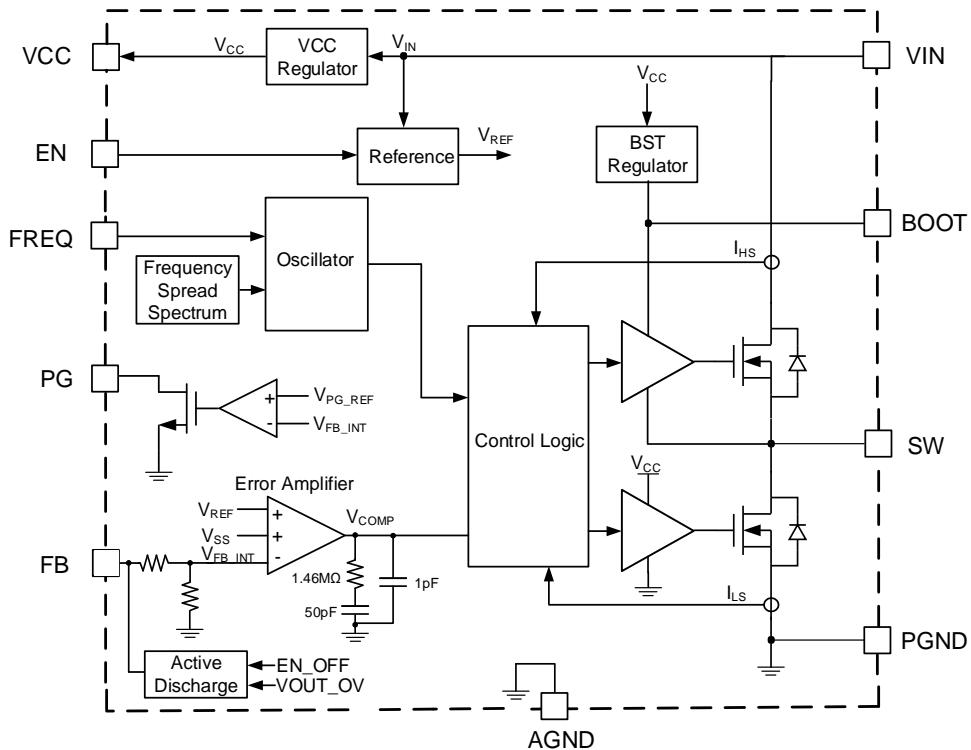


Figure 4: Functional Block Diagram (Fixed Output)

OPERATION

The MP4323C is a synchronous, step-down switching converter with integrated, internal high-side and low-side power MOSFETs (HS-FETs and LS-FETs, respectively). The device provides 3A of highly efficient output with peak current mode control.

The MP4323C features a wide input voltage range, configurable 350kHz to 2.5MHz switching frequency, internal soft start, and precision current limit. The device's low operational quiescent current suits makes it well-suited for battery-powered applications.

PWM Control

At moderate to high output currents, the MP4323C operates with fixed frequency, peak current mode control to regulate the output voltage. A PWM cycle is initiated by the internal clock. At the rising edge of the clock, the high-side MOSFET (HS-FET) turns on and remains on until the control signal reaches the value set by the internal COMP voltage (V_{COMP}).

When the HS-FET is off, the low-side MOSFET (LS-FET) turns on immediately. The LS-FET stays on until the next cycle starts, or until the inductor current (I_L) falls below the reverse current. The LS-FET remains off for at least the minimum off time before the next cycle starts.

If the current in the HS-FET cannot reach the value set by COMP within one PWM period, the HS-FET remains on and skips a turn-off operation. The HS-FET is forced off when it reaches the value set by COMP, or its 7 μ s maximum on time is reached. This operation mode extends the duty cycle, which achieves a low dropout when the input voltage (V_{IN}) is almost equal to the output voltage (V_{OUT}).

Light-Load Operation

Under light-load conditions, the MP4323C can work in forced continuous conduction mode (FCCM). In FCCM, the device works with a fixed frequency from no-load to full-load. The advantages of FCCM are its controllable frequency and lower output voltage ripple at light loads.

Error Amplifier

The error amplifier compares the FB pin's voltage (V_{FB}) with the internal reference (0.8V),

and outputs a current proportional to the difference between the two values. This output current is then used to charge the compensation network to form V_{COMP} , which is the error used to control the power MOSFET duty cycle.

During normal operation, the minimum V_{COMP} is clamped to 0.5V, and the maximum is clamped to 2.5V. COMP is internally pulled down to GND in shutdown mode.

Spread Spectrum

The MP4323C uses a 15kHz modulation frequency with a maximum 128-step triangular profile to spread the internal oscillator frequency across a 20% ($\pm 10\%$) window. The steps vary with the set oscillator frequency to ensure that the exact switching frequency steps cycle by cycle (see Figure 5).

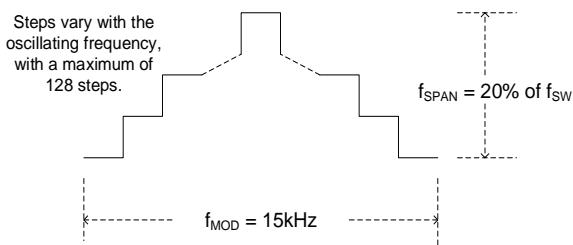


Figure 5: Spread Spectrum

Side bands are created by modulating the switching frequency with the triangle modulation waveform. The emission power of the fundamental switching frequency and its harmonics is reduced. This significantly reduces peak EMI noise.

Soft Start

Soft start is implemented to prevent the converter output voltage from overshooting during start-up. The soft-start time is fixed internally.

When the soft-start period starts, the soft-start voltage (V_{SS}) rises from 0V to 1.2V with a specific slew rate. When V_{SS} drops below the internal 0.8V reference voltage (V_{REF}), V_{SS} overrides V_{REF} , and the error amplifier uses V_{SS} as the reference. When V_{SS} exceeds V_{REF} , the error amplifier uses V_{REF} as the reference.

When the chip is enabled by EN, the first pulse is sent after 830 μ s. During this period, VCC is regulated, and the compensator network and

internal bias finish charging. After another 2.9ms, V_{OUT} ramps up and reaches its set value. Then soft start is completed after 1.5ms. PG is pulled high after a 70 μ s delay.

Pre-Biased Start-Up

If V_{FB} exceeds V_{SS} at start-up, this means the output has a pre-biased voltage. In this scenario, neither the HS-FET nor LS-FET turn on until V_{SS} exceeds V_{FB} .

Thermal Shutdown

Thermal shutdown is implemented to prevent the chip from thermal runaway. If the silicon die temperature rises above its upper threshold (about 175°C), the device shuts down the power MOSFETs. If the temperature drops below its lower threshold (about 155°C), the thermal shutdown condition is removed, and the chip is enabled again.

Peak and Valley Current Limit

Both the HS-FET and LS-FET have cycle-by-cycle current-limit protection. If the inductor current (I_L) reaches the high-side peak current limit (typically 5.8A) while the HS-FET is on, the HS-FET is forced off immediately to prevent the current from rising.

When the LS-FET is on, the next clock's rising edge is held until I_L drops below the low-side valley current limit (typically 4.4A). Then I_L can drop to a sufficiently low value when the HS-FET turns on again. This current limit scheme prevents current runaway if an overload or short-circuit event occurs.

Reverse Current Limit

The direction of the reverse current is from the output to the SW node. The MP4323C has a 3A reverse current limit. If the inductor current reaches the current limit, the LS-FET immediately turns off and the HS-FET turns on. The current limit prevents a negative current from dropping too low and damaging the components.

Short-Circuit Protection (SCP)

If the output is shorted to ground, and the output voltage drops below 70% of its nominal output, the MP4323C shuts down and begins discharging V_{SS} . The device restarts with a full soft start when V_{SS} is fully discharged. This hiccup process is repeated until the fault is removed.

Output Over-Voltage Protection (OVP) and Discharge

The MP4323C stops switching if V_{OUT} exceeds 130% of its nominal regulation value, and an internal 75Ω discharge path from FB to GND is activated to discharge V_{OUT} . This discharge path can only be activated if the output is fixed. The part resumes switching when V_{OUT} drops below 125% of its nominal value, and then the discharge path is disabled.

For fixed output versions, the V_{OUT} discharge path is also activated if an EN shutdown occurs while V_{CC} exceeds its under-voltage lockout (UVLO) threshold. When V_{CC} drops below its UVLO threshold, this path is deactivated.

Start-Up and Shutdown

If both V_{IN} and EN exceeds their appropriate thresholds, the chip starts up. The reference block starts first, generating a stable reference voltage and currents, and then the internal regulator is enabled. The regulator provides a stable supply for the remaining circuitries.

When the internal supply rail is up, the internal circuits start to work. If BOOT does not reach its refresh rising threshold (about 2.5V), the LS-FET turns on to charge BOOT. The HS-FET stays off during this time. When the soft-start block is enabled, V_{OUT} starts to ramp up slowly. V_{OUT} smoothly reaches its target within 5ms.

Three events can shut down the chip: EN going low, V_{IN} falling below its UVLO threshold, and thermal shutdown. During shutdown, the signaling path is blocked first to avoid any fault triggering. Then the COMP voltage is pulled down, and the floating driver works to disable the HS-FET.

APPLICATION INFORMATION

Figure 6 shows the MP4323C's typical application circuit.

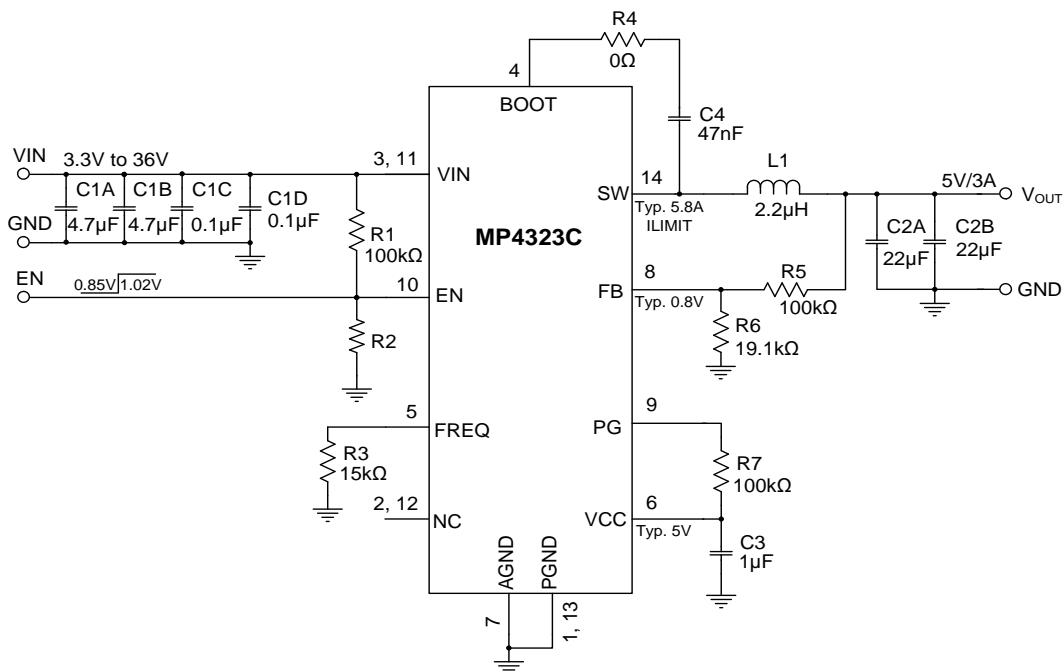


Figure 6: Typical Application Circuit ($V_{OUT} = 5V$, $f_{sw} = 2.2\text{MHz}$)

Table 1: Design Guide Index

Pin #	Pin Name	Component	Design Guide Index
1, 13	PGND		GND Connection (Pins 1, 7, and 13)
2, 12	NC		No Connection (NC, Pins 2 and 12)
3, 11	VIN	C1A, C1B, C1C, C1D	Selecting the Input Capacitors (VIN, Pins 3 and 11)
4	BOOT	R4, C4	Floating Driver and Bootstrap Charging (BOOT, Pin 4)
5	FREQ	R3	Setting the Switching Frequency (FREQ, Pin 5)
6	VCC	C3	Internal VCC (VCC, Pin 6)
7	AGND		GND, Connection GND
8	FB	R5, R6	Feedback (FB, Pin 8)
9	PG	R7	Power Good Indicator (PG, Pin 9)
10	EN	R1, R2	Enable and Under-Voltage Lockout (UVLO) (EN, Pin 10)
14	SW	L1, C2A, C2B	Selecting the Inductor and Output Capacitors (SW, Pin 14)

Selecting the Input Capacitors (VIN, Pins 3 and 11)

The step-down converter has a discontinuous input current, and requires a capacitor to supply AC current to the converter while maintaining the DC input voltage. For the best performance, use low-ESR capacitors. Ceramic capacitors with X5R or X7R dielectrics are highly recommended because of their low ESR and small temperature coefficients.

For most applications, use a $4.7\mu\text{F}$ to $10\mu\text{F}$ capacitor. It is strongly recommended to use an additional lower-value capacitor (e.g. $0.1\mu\text{F}$) with a small package size (0603) to absorb high-frequency switching noise. Place the smaller capacitor as close to VIN and GND as possible.

Since the input capacitor (C_{IN}) absorbs the input switching current, it requires an adequate ripple current rating. The RMS current in the input capacitor can be estimated with Equation (1):

$$I_{CIN} = I_{LOAD} \times \sqrt{\frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)} \quad (1)$$

The worst-case condition occurs at $V_{IN} = 2 \times V_{OUT}$, calculated with Equation (2):

$$I_{CIN} = \frac{I_{LOAD}}{2} \quad (2)$$

For simplification, choose an input capacitor with an RMS current rating greater than half of the maximum load current. The input capacitor can be electrolytic, tantalum, or ceramic. When using electrolytic or tantalum capacitors, add a small, high-quality ceramic capacitor (e.g. $0.1\mu\text{F}$) as close to the IC as possible. When using ceramic capacitors, ensure that they have enough capacitance to provide a sufficient charge to prevent excessive voltage ripple at the input. The input voltage ripple caused by the capacitance can be estimated with Equation (3):

$$\Delta V_{IN} = \frac{I_{LOAD}}{f_{SW} \times C_{IN}} \times \frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \quad (3)$$

V_{IN} Over-Voltage Protection (OVP)

The MP4323C stops switching when V_{IN} rises above its over-voltage (OV) rising threshold (typically 37.5V). The device resumes normal

regulation and switching when V_{IN} drops below the OV falling threshold (typically 36.5V).

Floating Driver and Bootstrap Charging (BOOT, Pin 4)

The BOOT capacitor (C_4 , also called C_{BOOT}) is recommended to be between 22nF and 100nF .

It is not recommended to place a resistor (R_{BOOT}) in series with the BOOT capacitor, unless there is a strict EMI requirement. Although R_{BOOT} helps enhance EMI performance and reduces voltage stress at higher input voltages, it also generates additional power consumption and reduces efficiency. If R_{BOOT} is required, it should be set below 4Ω .

The voltage between BOOT and SW ($V_{BOOT-SW}$) is regulated to about 5V by the dedicated internal bootstrap regulator. When $V_{BOOT-SW}$ is below its regulation value, an N-channel MOSFET pass transistor connected from VCC to BOOT turns on to charge the bootstrap capacitor (C_{BOOT}). The external circuit should provide enough voltage headroom to facilitate charging. When the HS-FET is on, the BOOT voltage exceeds V_{CC} , and the bootstrap capacitor cannot be charged. At higher duty cycles, the time available for the bootstrap capacitor to charge is shorter, and it may not charge sufficiently. If the external circuit has insufficient voltage and time to charge the bootstrap capacitor, additional external circuitry can be used to ensure that the bootstrap voltage remains in the normal operation region.

If the bootstrap voltage reaches its under-voltage lockout (UVLO) threshold, the HS-FET turns off. The LS-FET turns on with a minimum off time to refresh the bootstrap voltage with the set f_{SW} .

Setting the Switching Frequency (FREQ, Pin 5)

A resistor (R_3) can set the switching frequency (see Table 2 on page 30 and the f_{SW} vs. R_{FREQ} curves on page 14).

The switching frequency can be configured by an external resistor (R_{FREQ}) connected from the FREQ pin to ground. The frequency resistor should be located between the FREQ pin and GND, and placed as close as possible to the device. Table 2 on page 30 shows the relationship between the switching frequency and R_{FREQ} .

Table 2: f_{SW} vs. R_{FREQ}

R _{FREQ} (kΩ)	f _{SW} (kHz)	R _{FREQ} (kΩ)	f _{SW} (kHz)
100	355	30.1	1150
93.1	385	26.1	1300
86.6	415	22.6	1450
80.6	450	20.5	1600
75	480	19.6	1750
68.1	520	17.8	1900
59	600	16.2	2050
51.1	700	15	2200
40.2	850	14.3	2350
34.8	1000	13.3	2500

It is not possible to have both a high switching frequency and a high input voltage due to the HS-FET's limited minimum on time. The MP4323C control loop automatically sets the maximum possible f_{SW} to the set frequency, which also reduces excessive power loss. V_{OUT} is regulated by varying the duration of the HS-FET's switch off time, which automatically reduces f_{SW}.

The device is guaranteed to comply with the HS-FET's minimum on time. An advantage of this method is that the device works at the target f_{SW} for as long as possible, and f_{SW} only changes when the device operates at high input voltages. For more details, see the f_{SW} vs. V_{IN} curve on page 14. In this scenario, R_{FREQ} = 15kΩ, and V_{OUT} = 3.3V.

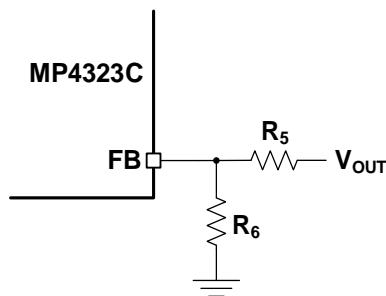
Internal VCC (VCC, Pin 6)

The VCC capacitor (C3) is recommended to be 1μF.

Most of the internal circuitry is powered by the internal 5V VCC regulator. This regulator uses V_{IN} as its input and operates across the full V_{IN} range. When V_{IN} exceeds 5V, VCC is in full regulation. When V_{IN} drops below 5V, the VCC output degrades.

Feedback (FB, Pin 8)

The feedback voltage is typically 0.8V, and its output can be adjusted. The external resistor divider connected to FB sets the output voltage (see Figure 7).


Figure 7: Feedback Divider Network (Adjustable Output)

Calculate R₆ with Equation (4):

$$R_6 = \frac{R_5}{\frac{V_{OUT}}{0.8V} - 1} \quad (4)$$

For a fixed output, the FB resistor divider is integrated internally. This means that FB should be directly connected to the output to set the output voltage. The following fixed outputs can be selected: 1V, 1.8V, 2.5V, 3.0V, 3.3V, 3.8V, and 5V (see Figure 8).

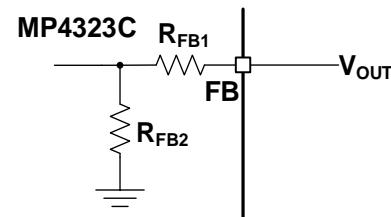

Figure 8: Feedback Divider Network (Fixed Output)

Table 3 shows the relationship between the internal R_{FB} and V_{OUT}.

Table 3: R_{FB} vs. V_{OUT}

V _{OUT} (V)	R _{FB1} (kΩ)	R _{FB2} (kΩ)
1	64	256
1.8	320	256
2.5	544	256
3.0	704	256
3.3	800	256
3.8	960	256
5	1344	256

Power Good Indicator (PG, Pin 9)

The PG resistor (R7) should have a resistance (R_{PG}) that is about 100kΩ.

The MP4323C includes an open-drain power

good (PG) output that indicates whether the regulator output is within the specific window of its nominal value.

If using PG, connect it to a logic high power source (e.g. 3.3V) through a pull-up resistor. PG goes high if the output voltage is within 94.5% to 105.5% of the nominal voltage; PG goes low if the output voltage is above 107% or below 93% of the nominal voltage. Float PG if it is not used.

Enable and Under-Voltage Lockout (UVLO) (EN, Pin 10)

EN is a digital control pin that turns the regulator on and off.

Enabled by the External Logic High/Low Signal

When the EN voltage reaches 0.7V, BG does not turn on until V_{IN} exceeds 2.7V. BG then provides an accurate reference voltage for the EN threshold. Forcing EN above its rising threshold (about 1.02V) turns the device on. Turn the device off by driving EN below 0.85V. There is no internal pull-up or pull-down resistor connected to the EN pin, so do not float EN. An external pull-up or pull-down resistor is required if the control signal cannot provide an accurate high or low logic.

Configurable V_{IN} Under-Voltage Lockout (UVLO)

The MP4323C has an internal, fixed under-voltage lockout (UVLO) threshold. The rising threshold is 3.65V, while the falling threshold is about 2.9V. For applications that require a higher UVLO point, an external resistor divider can be placed between V_{IN} and EN to raise the equivalent UVLO threshold (see Figure 9).

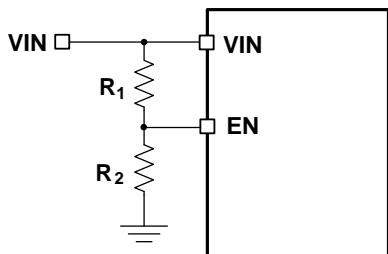


Figure 9: Adjustable UVLO Using EN Divider

The UVLO rising threshold can be calculated with Equation (5):

$$INUV_{RISING} = (1 + \frac{R_1}{R_2}) \times V_{EN_RISING} \quad (5)$$

Where V_{EN_RISING} is 1.02V.

The UVLO falling threshold can be estimated with Equation (6):

$$INUV_{FALLING} = (1 + \frac{R_1}{R_2}) \times V_{EN_FALLING} \quad (6)$$

Where $V_{EN_FALLING}$ is 0.85V.

If EN is not used to control when the device turns on and off, connect EN to a high voltage source (e.g. V_{IN}) to turn the device on by default.

Selecting the Inductor and Output Capacitors (SW, Pin 14)

The inductor (L_1) value can be estimated with Equation (7):

$$L_1 = \frac{V_{OUT}}{f_{SW} \times \Delta I_L} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \quad (7)$$

Where ΔI_L is the peak-to-peak inductor ripple current.

For most applications, it is recommended to use a 1 μ H to 10 μ H inductor with a DC current rating at least 25% higher than the maximum load current. For higher efficiency, choose an inductor with a lower DC resistance. A larger-value inductor results in less ripple current and a lower output ripple voltage, but also has a larger physical size, higher series resistance, and lower saturation current. A good rule to determine the inductor value is to allow the inductor ripple current to be approximately 30% of the maximum load current.

The peak inductor current (I_{LP}) value can be calculated with Equation (8):

$$I_{LP} = I_{LOAD} + \frac{V_{OUT}}{2 \times f_{SW} \times L} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \quad (8)$$

Choose an inductor that does not saturate under the peak inductor current.

The output voltage ripple can be estimated with Equation (9):

$$\Delta V_{OUT} = \frac{V_{OUT}}{f_{SW} \times L} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \times \left(R_{ESR} + \frac{1}{8 \times f_{SW} \times C_{OUT}}\right) \quad (9)$$

Where L is the inductor value, and R_{ESR} is the output capacitor's equivalent series resistance (ESR). The output capacitor (C_{OUT}) maintains the DC output voltage. Use ceramic, tantalum, or

low-ESR electrolytic capacitors. For the best results, use low-ESR capacitors to keep the output voltage ripple low.

For ceramic capacitors, the capacitance dominates the impedance at the switching frequency and causes most of the output voltage ripple. For simplification, the output voltage ripple can be calculated with Equation (10):

$$\Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{8 \times f_{\text{SW}}^2 \times L \times C_{\text{OUT}}} \times \left(1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}\right) \quad (10)$$

For tantalum or electrolytic capacitors, the ESR dominates the impedance at the switching frequency. For simplification, the output voltage ripple can be estimated with Equation (11):

$$\Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{f_{\text{SW}} \times L} \times \left(1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}\right) \times R_{\text{ESR}} \quad (11)$$

When selecting an output capacitor, consider the allowable overshoot in V_{OUT} if the load is suddenly removed. In this scenario, energy stored in the inductor is transferred to C_{OUT} , causing its voltage to rise. To achieve an optimal overshoot relative to the regulated voltage, the output capacitance can be estimated with Equation (12):

$$C_{\text{OUT}} = \frac{I_{\text{OUT}}^2 \times L}{V_{\text{OUT}}^2 \times ((V_{\text{OUTMAX}}/V_{\text{OUT}})^2 - 1)} \quad (12)$$

Where $V_{\text{OUTMAX}}/V_{\text{OUT}}$ is the allowable maximum overshoot. After calculating the capacitance that meets both the ripple and overshoot requirements, choose the greater capacitance value.

The characteristics of the output capacitor also affect the stability of the regulation system. The MP4323C can be optimized for a wide range of capacitance and ESR values.

GND Connection (Pins 1, 7, and 13)

See the PCB Layout Guidelines on page 33 for more details.

PCB Layout Guidelines ⁽¹³⁾

Efficient PCB layout, especially input capacitor placement, is critical for stable operation. A four-layer layout is strongly recommended to improve thermal performance. For the best results, refer to Figure 10 and follow the guidelines below:

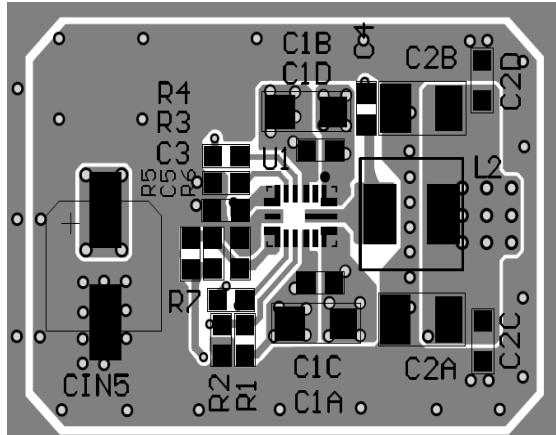
1. Place symmetric input capacitors as close to VIN and GND as possible.
2. Use a large ground plane to connect directly to PGND.
3. Add vias near PGND if the bottom layer is a ground plane.
4. Ensure that the high-current paths at GND and VIN have short, direct, and wide traces.
5. Place the ceramic input capacitor, especially the small package size (0603) input bypass

capacitor, as close to VIN and PGND as possible to minimize high-frequency noise.

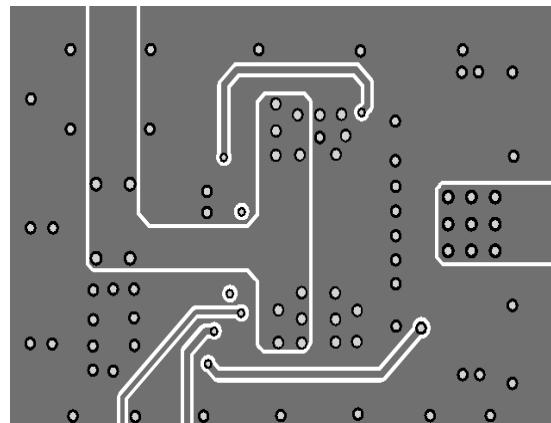
6. Keep the connection between the input capacitor and VIN as short and wide as possible.
7. Place the VCC capacitor as close to VCC and AGND as possible.
8. Route SW and BOOT away from sensitive analog areas, such as FB.
9. Place the feedback resistors close to the chip to ensure the trace that connects to FB is as short as possible.
10. Use multiple vias to connect the power planes to the internal layers.

Note:

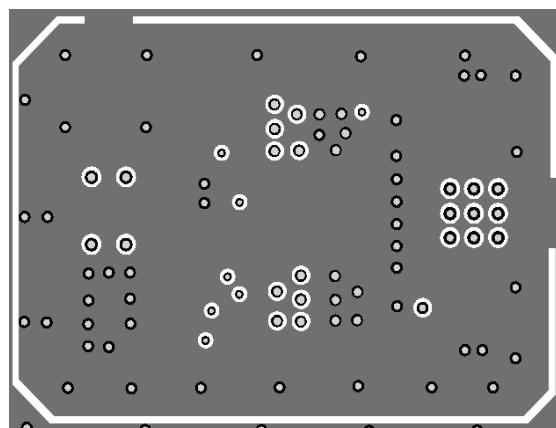
13) The recommended PCB layout is based on Figure 6 on page 28.



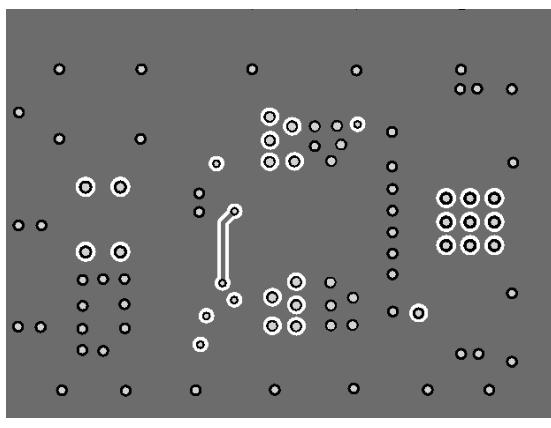
Top Silk and Top Layer



Mid-Layer 2



Mid-Layer 1



Bottom Layer and Bottom Silk

Figure 10: Recommended PCB Layout

TYPICAL APPLICATION CIRCUITS

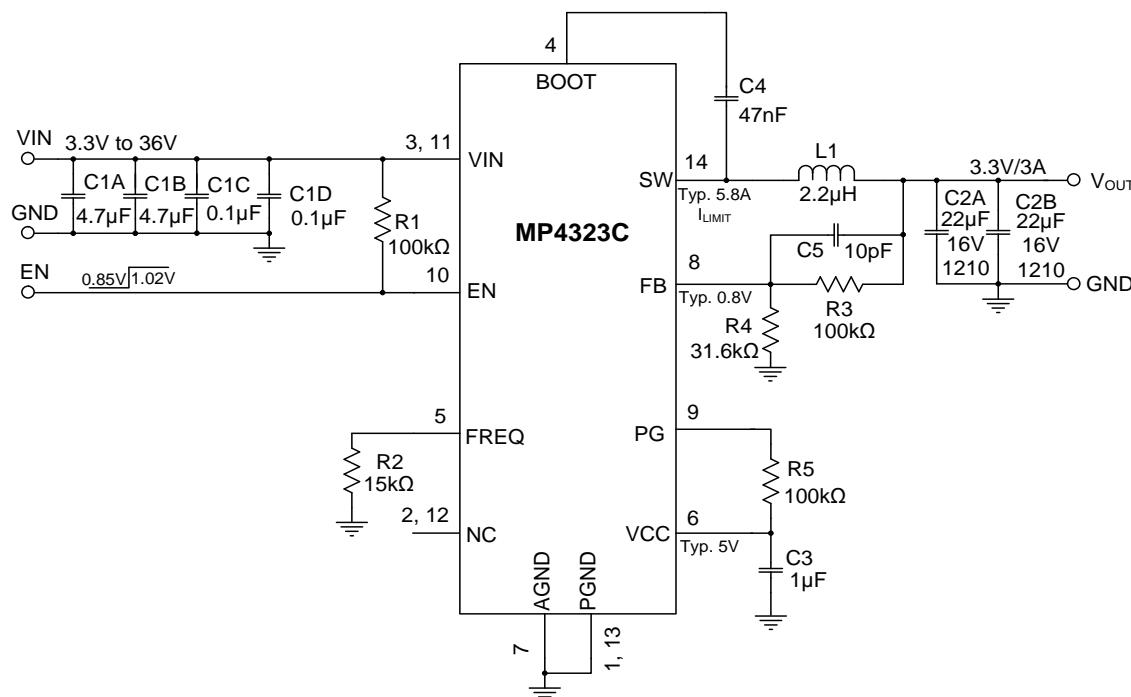


Figure 11: Typical Application Circuit ($V_{OUT} = 3.3V$, $f_{sw} = 2.2MHz$)

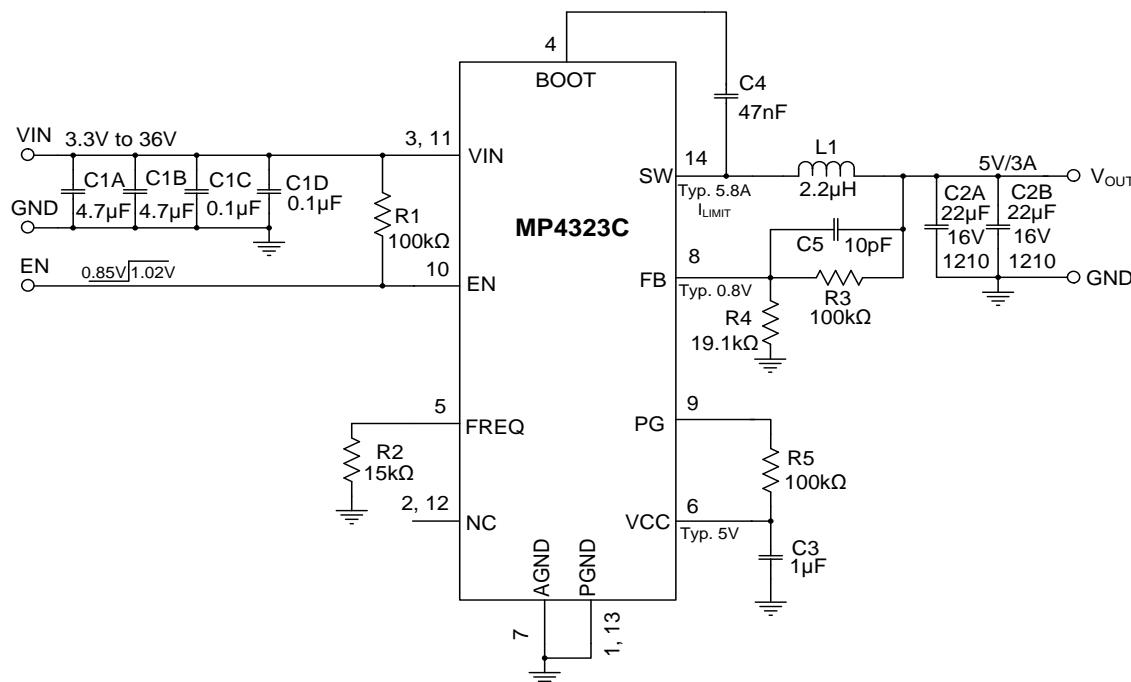


Figure 12: Typical Application Circuit ($V_{OUT} = 5V$, $f_{sw} = 2.2MHz$)

TYPICAL APPLICATION CIRCUITS (continued)

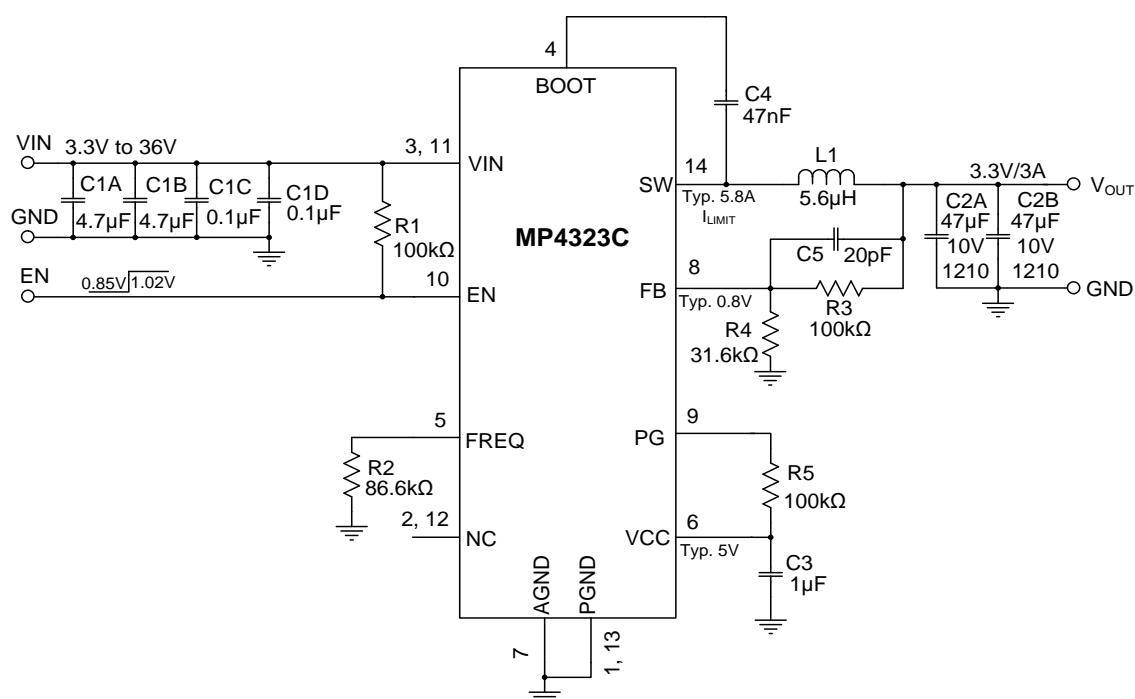


Figure 13: Typical Application Circuit ($V_{OUT} = 3.3V$, $f_{sw} = 415kHz$)

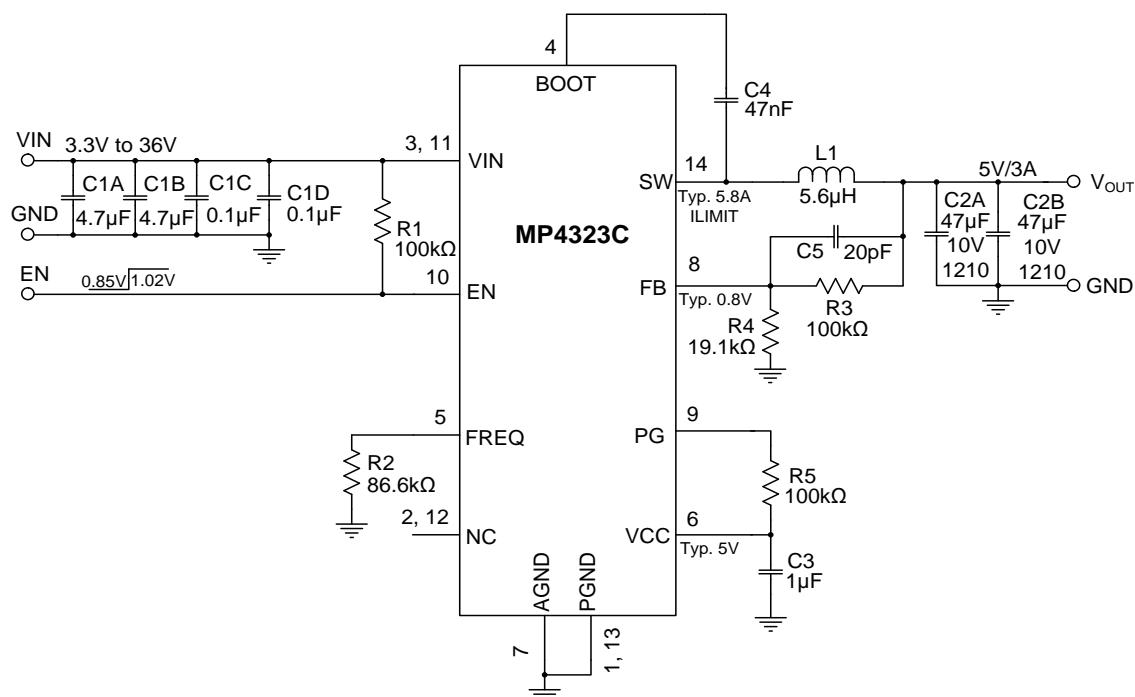


Figure 14: Typical Application Circuit ($V_{OUT} = 5V$, $f_{sw} = 415kHz$)

TYPICAL APPLICATION CIRCUITS (continued)

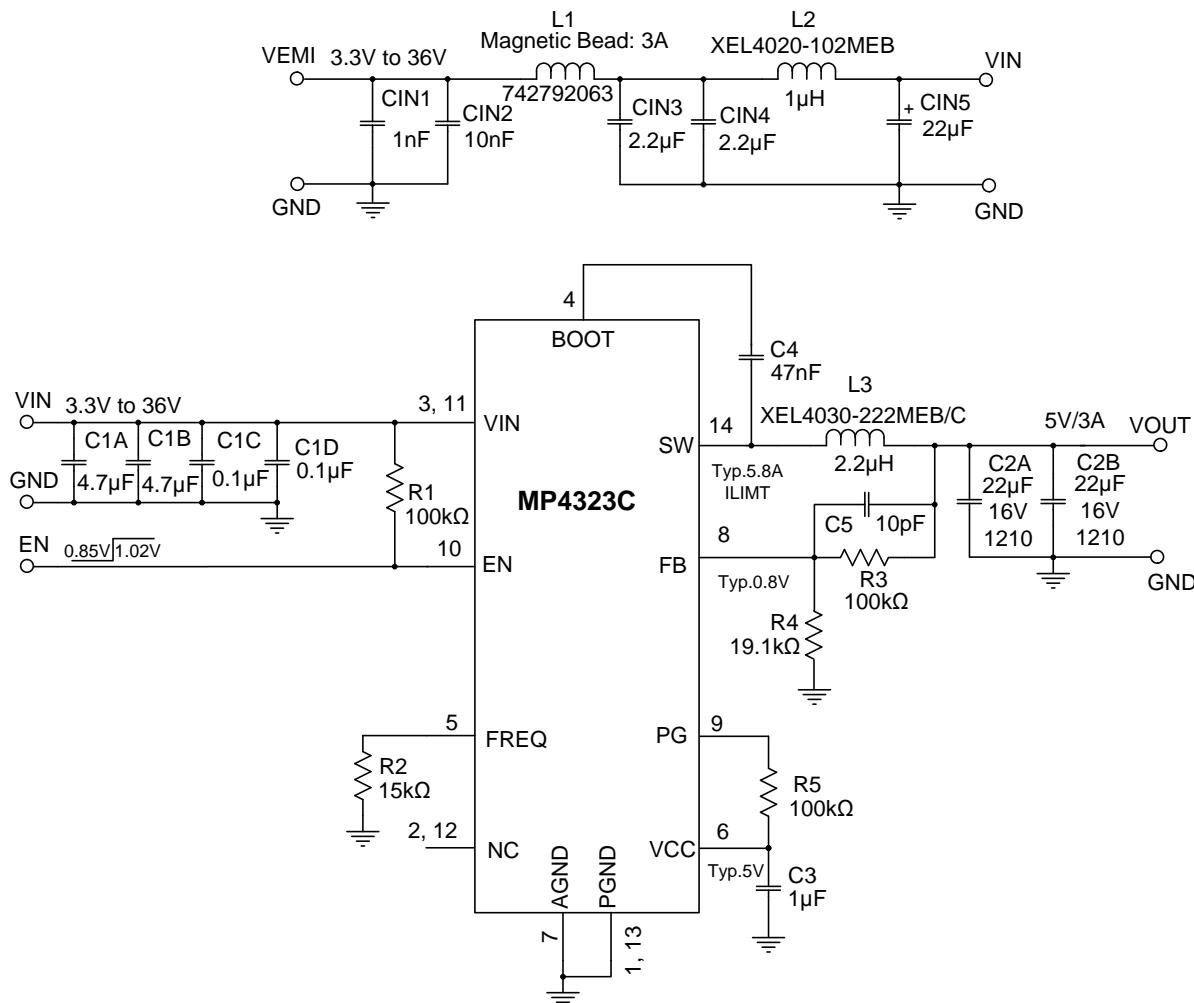


Figure 15: Typical Application Circuit ($V_{OUT} = 5V$, $f_{sw} = 2.2\text{MHz}$ with EMI Filters)

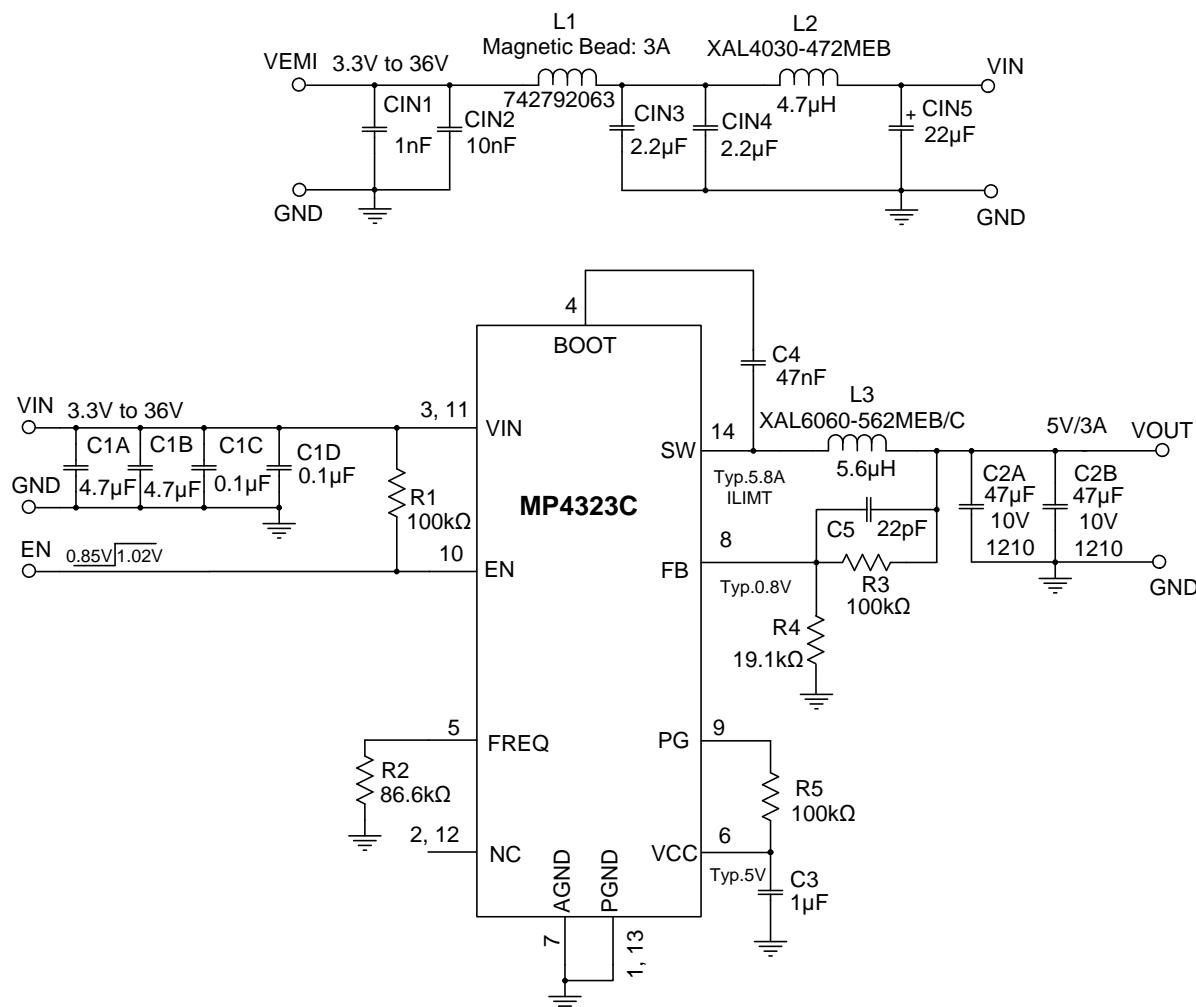
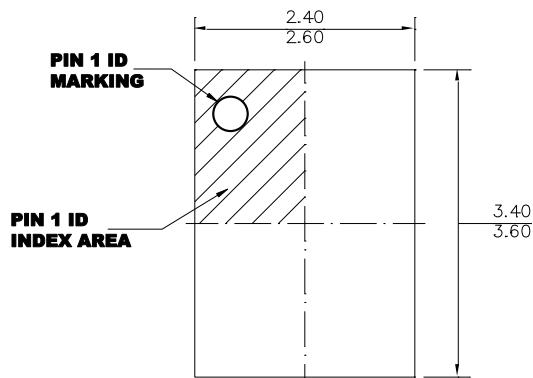
TYPICAL APPLICATION CIRCUITS (*continued*)


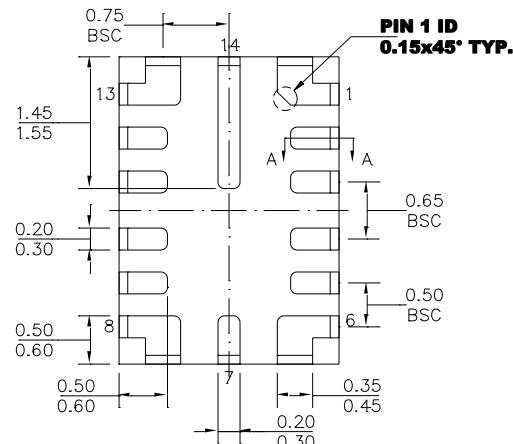
Figure 16: Typical Application Circuit ($V_{OUT} = 5V$, $f_{sw} = 415kHz$ with EMI Filters)

PACKAGE INFORMATION

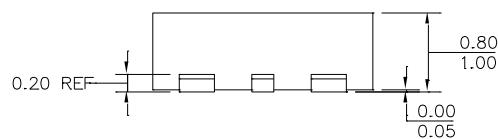
**QFN-14 (2.5mmx3.5mm)
Wettable Flank**



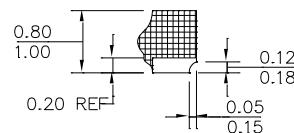
TOP VIEW



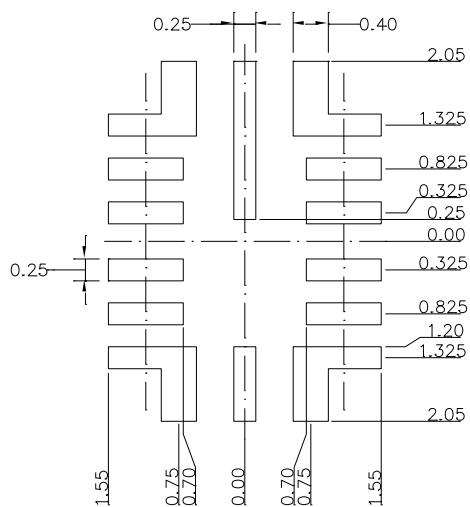
BOTTOM VIEW



SIDE VIEW



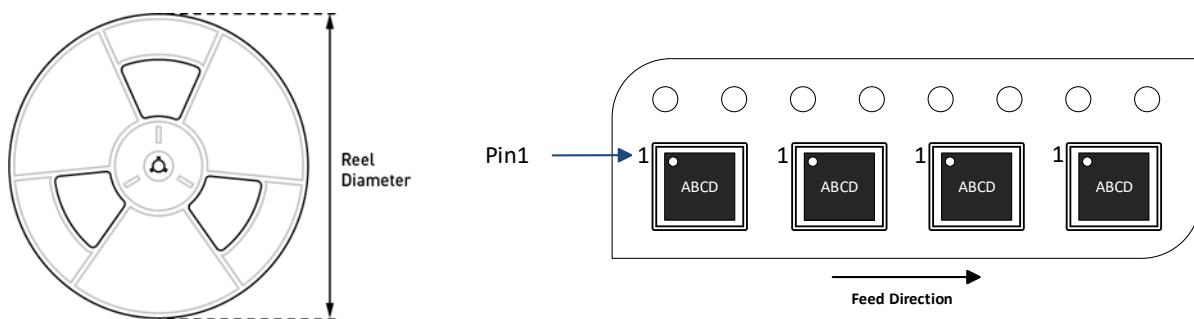
SECTION A-A



RECOMMENDED LAND PATTERN

NOTE:

- 1) THE LEAD SIDE IS WETTABLE.
- 2) ALL DIMENSIONS ARE IN MILLIMETERS.
- 3) LEAD COPLANARITY SHALL BE 0.08 MILLIMETERS MAX.
- 4) JEDEC REFERENCE IS MO-220.
- 5) DRAWING IS NOT TO SCALE.

CARRIER INFORMATION

Part Number	Package Description	Quantity/Reel	Quantity/Tube	Quantity/Tray	Reel Diameter	Carrier Tape Width	Carrier Tape Pitch
MP4323CGRHE-Z	QFN-14 (2.5mmx3.5mm)	5000	N/A	N/A	13in	12mm	8mm

REVISION HISTORY

Revision #	Revision Date	Description	Pages Updated
1.0	08/26/2021	Initial Release	-
1.1	5/15/2023	Removed “(Absolute Maximum)” in Features section	1
		Updated the minimum start-up V_{IN} from 3.8V to 3.9V; added detail description about θ_{JC} in note and note 8	5
		Updated “PG rising/falling delay” to “PG rising/falling deglitch time”; minor formatting updates	7
		Updated recommended C_{BOOT} to “22nF to 100nF”; updated “P-channel MOSFET” to “N-channel MOSFET”	29
		Updated the Recommended PCB Layout (Figure 10); formatting updates.	33
		Updated C4 from “100nF” to “47nF” in Figure 6, Figure 11, Figure 12, Figure 13, Figure 14, Figure 15, and Figure 16	28, 34–37

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